

# **PWR Vessel Through Wall Crack Frequency based on Realistic Crack Assessment and its Implications for In-service Inspection**

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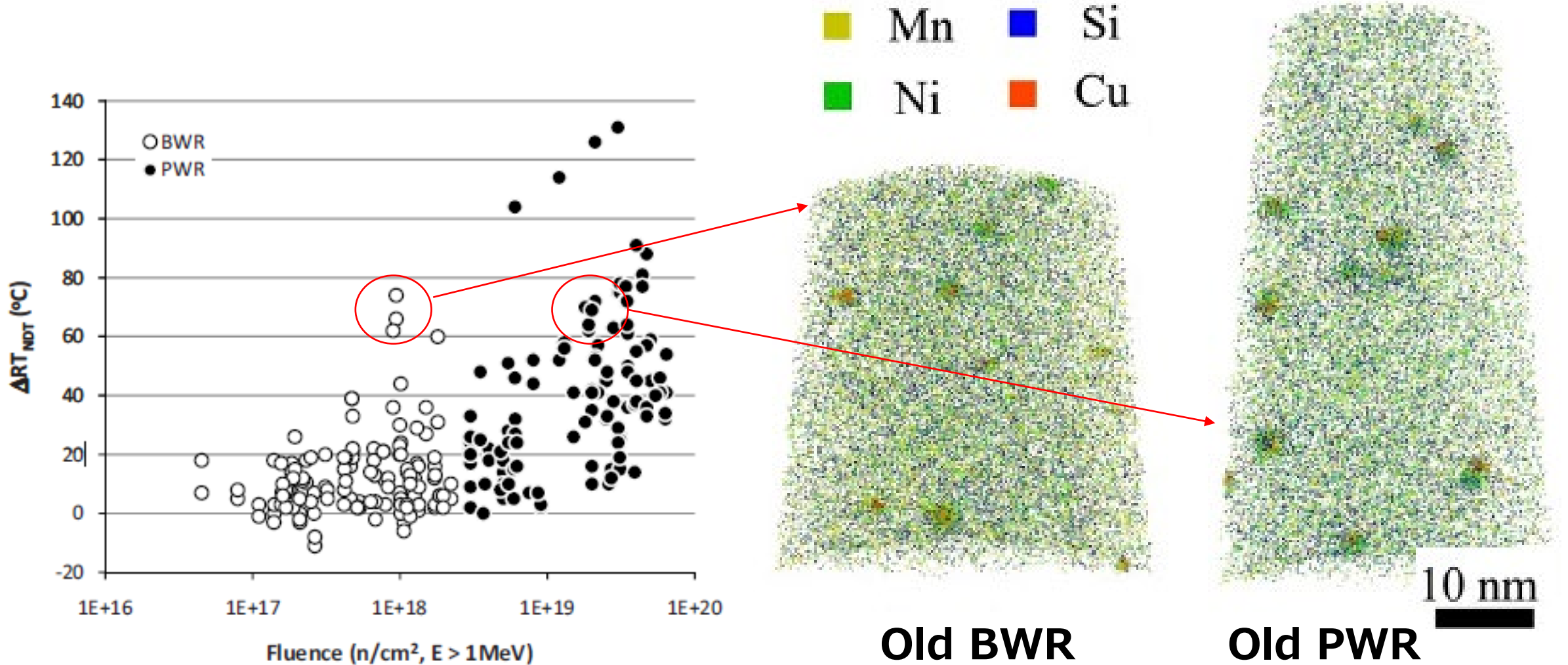
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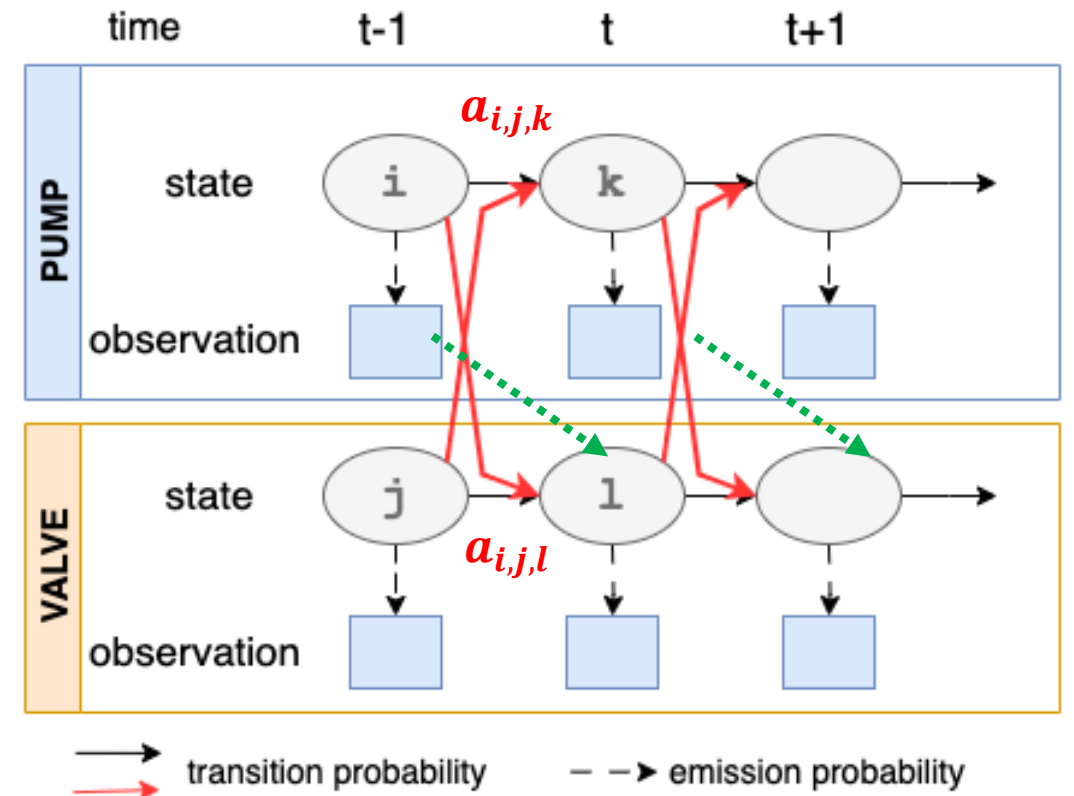
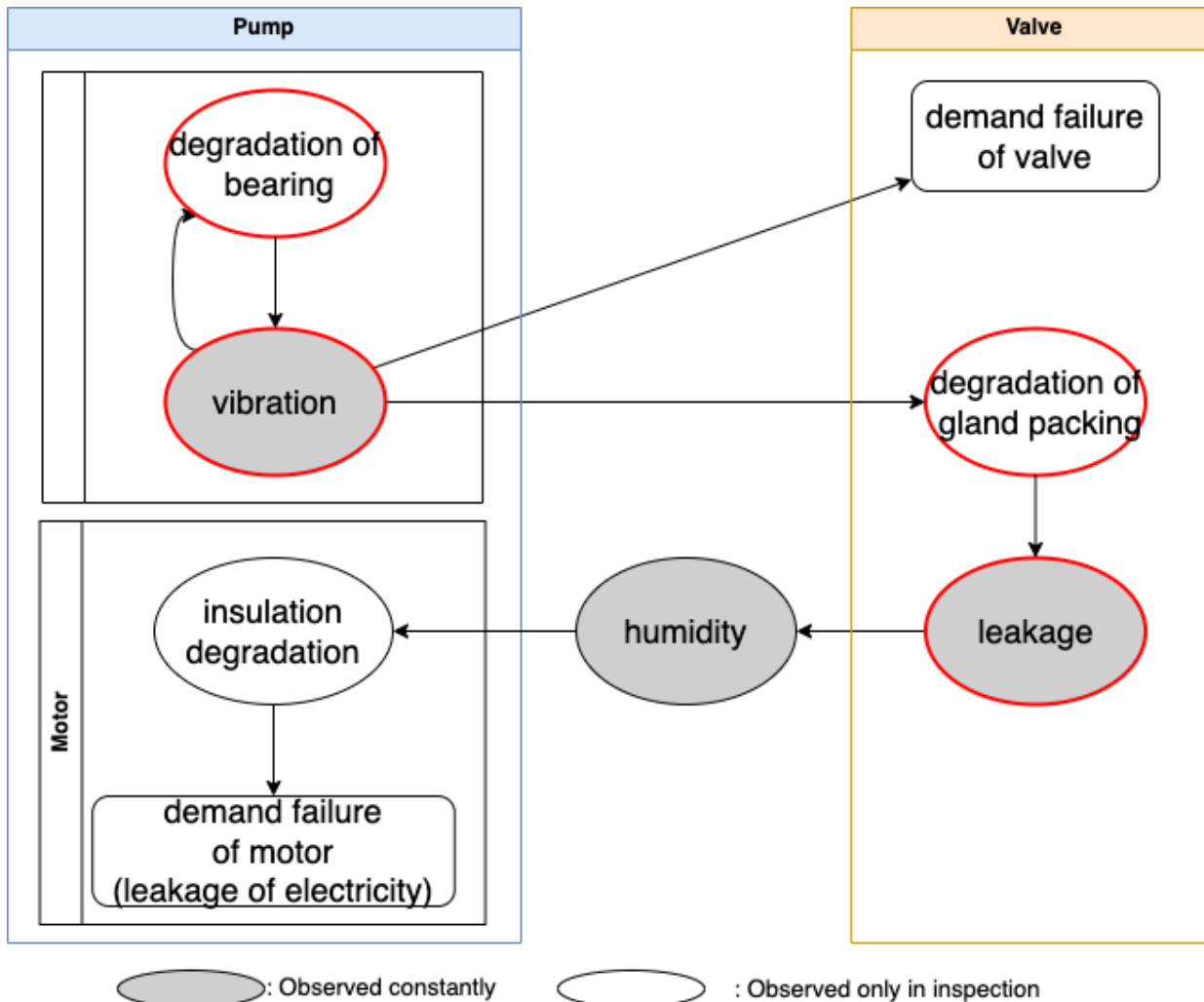
# Introduction of the Lab (1)

Material research for safety, especially the safe LTO



# Introduction of the Lab (2)

## Risk-informed decision making for O&M



# Background: Reinforcement of ISI in Japan

- Special Inspection for LTO @ 40y (and 80y)
  - Requires UT for all region (base, weld) in beltline
- Endorsement of JSME S NA1 (ver 2012-14) :
  - The area and frequency of Ultrasonic Testing for RPV welding line were reinforced from 7.5%/T to 100%/T
    - T = 10 year (by 30 years old) 、 T = 7 year (> 30 years old)

# Research Questions

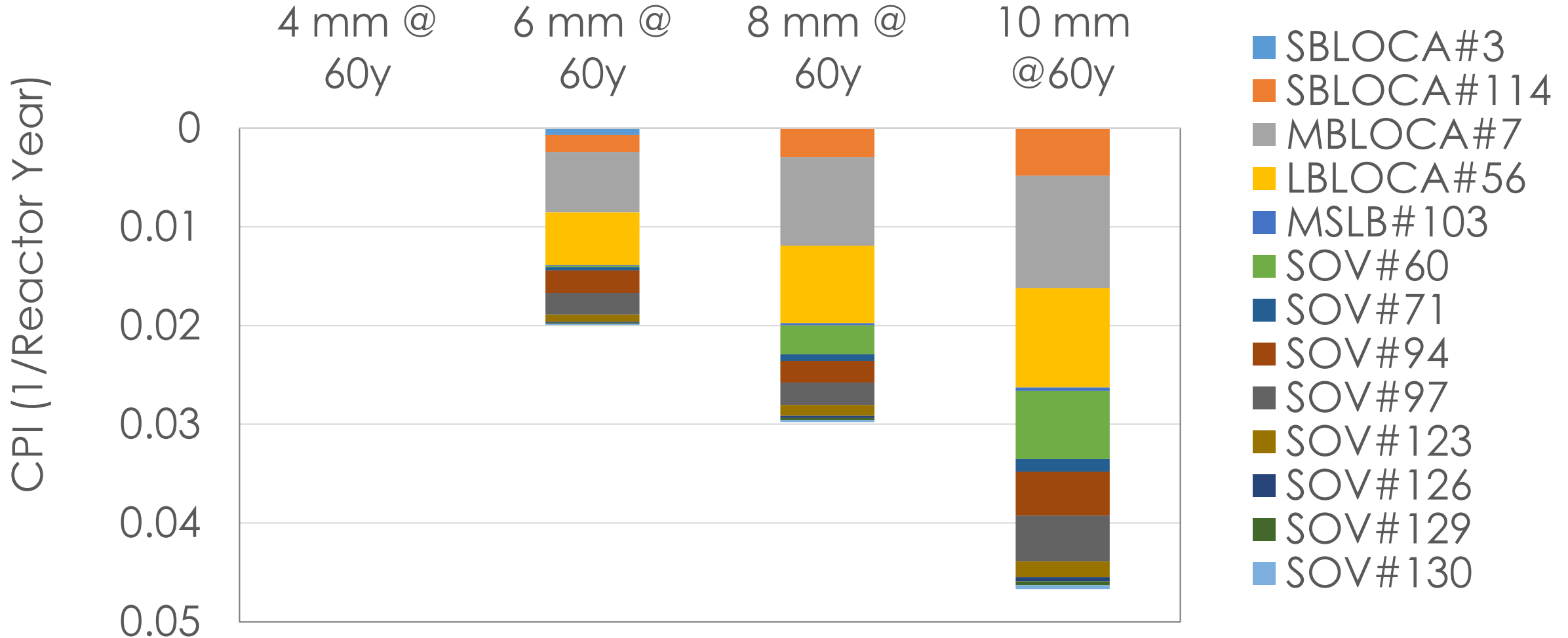
- How ISI can be justified theoretically?
  1. Very small crack, overlooked pre-operational inspection, may be **grown by fatigue** and may be found by the ISI
  2. Reduction of fracture toughness by neutron irradiation can be **compensated by ISI, limiting/reducing the crack probability**
- Effect of **crack distribution changes along time** is demonstrated and Rationality of ISI reinforcement may be evaluated.

# Analysis : PASCAL-5, Referring JAEA-Data/Code 2022-006

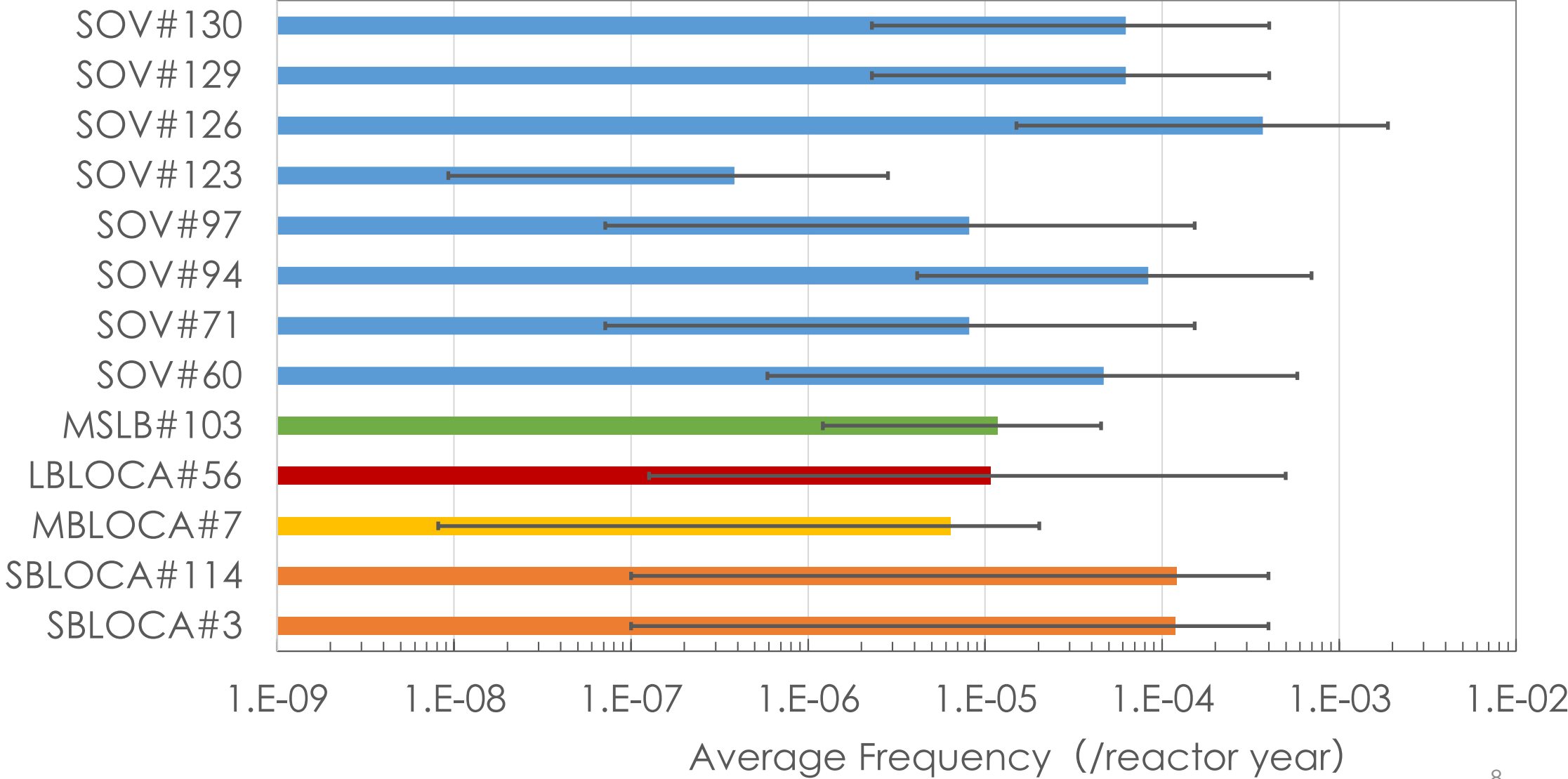
- Information of RPV
  - Size: Conventional 3-loop PWR
  - $RT_{NDT}$ : Base: around 90°C, Weld: around 50°C @ 60y
    - Base : Initial  $RT_{NDT} = -5^{\circ}\text{C}$ , 0.16%Cu, 0.61%Ni (median)
    - Weld : Initial  $RT_{NDT} = -50^{\circ}\text{C}$ , 0.14%Cu, 0.80%Ni (median)
    - Embrittlement Trend Curve: JEAC4201-2007 (2013 addendum), Fast neutron fluence is  $7 \times 10^{19}$  n/cm<sup>2</sup> @ 60y.
- Crack distribution
  - Initial distribution: VFLAW, considering Japanese PWR welding
  - Stress history and crack growth: JSME S-ND1 + Paris Law
  - Non-distractive testing: Bayesian update, POD H/M/L

# Conditional Probability for Crack Initiation for Deterministic Embedded Cracks

Uncertainty for fracture toughness were taken into account

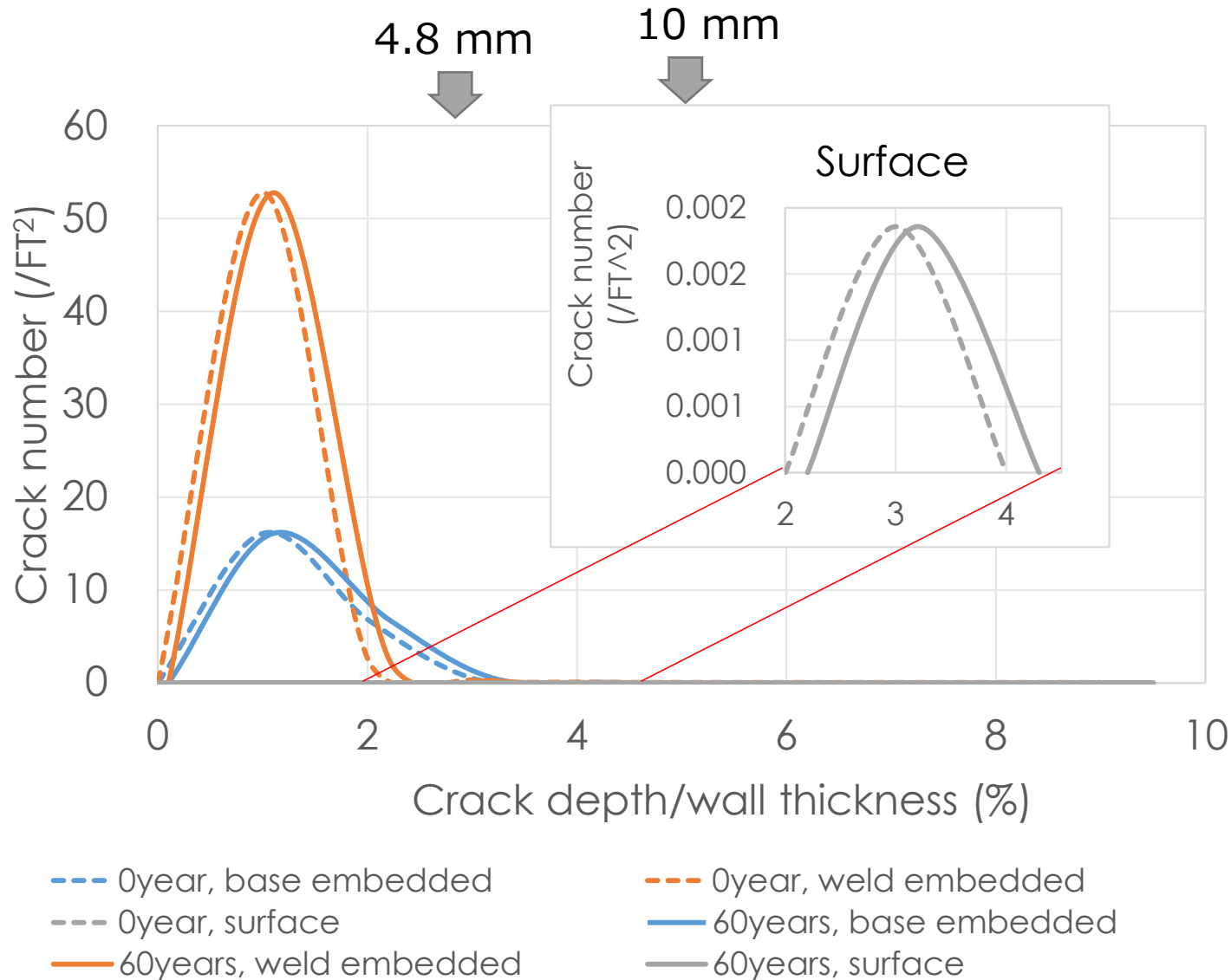


# 13 Transients selected based on NUREG-1806



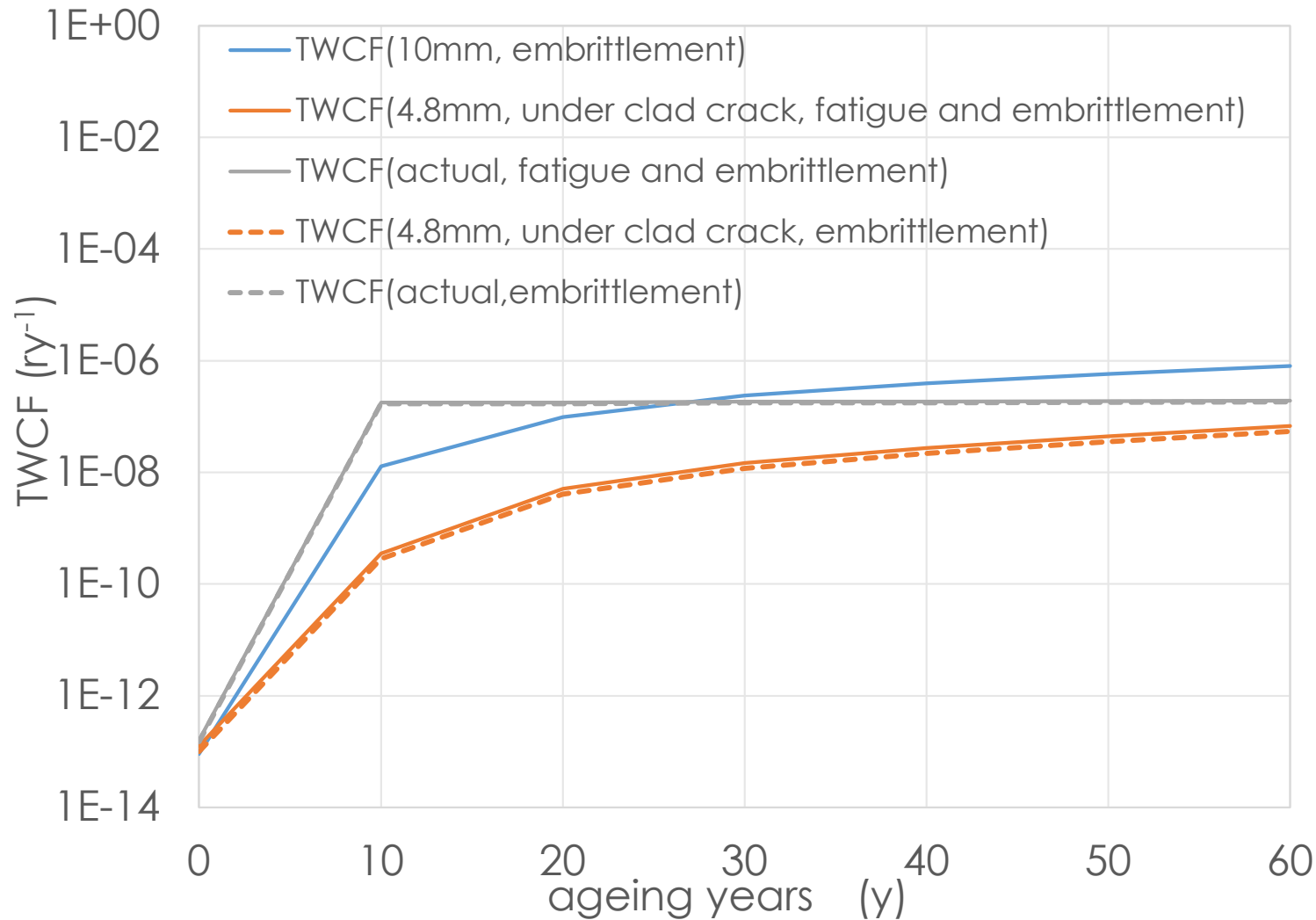


# Crack Growth by Fatigue



- Surface crack is 3 order smaller than embedded crack
- Crack size change is smaller than 1% (=2mm) of the thickness of wall  
 → The change has to be considered by stress intensity factor
- Crack size would be smaller than 6 mm after 60 years of operation.

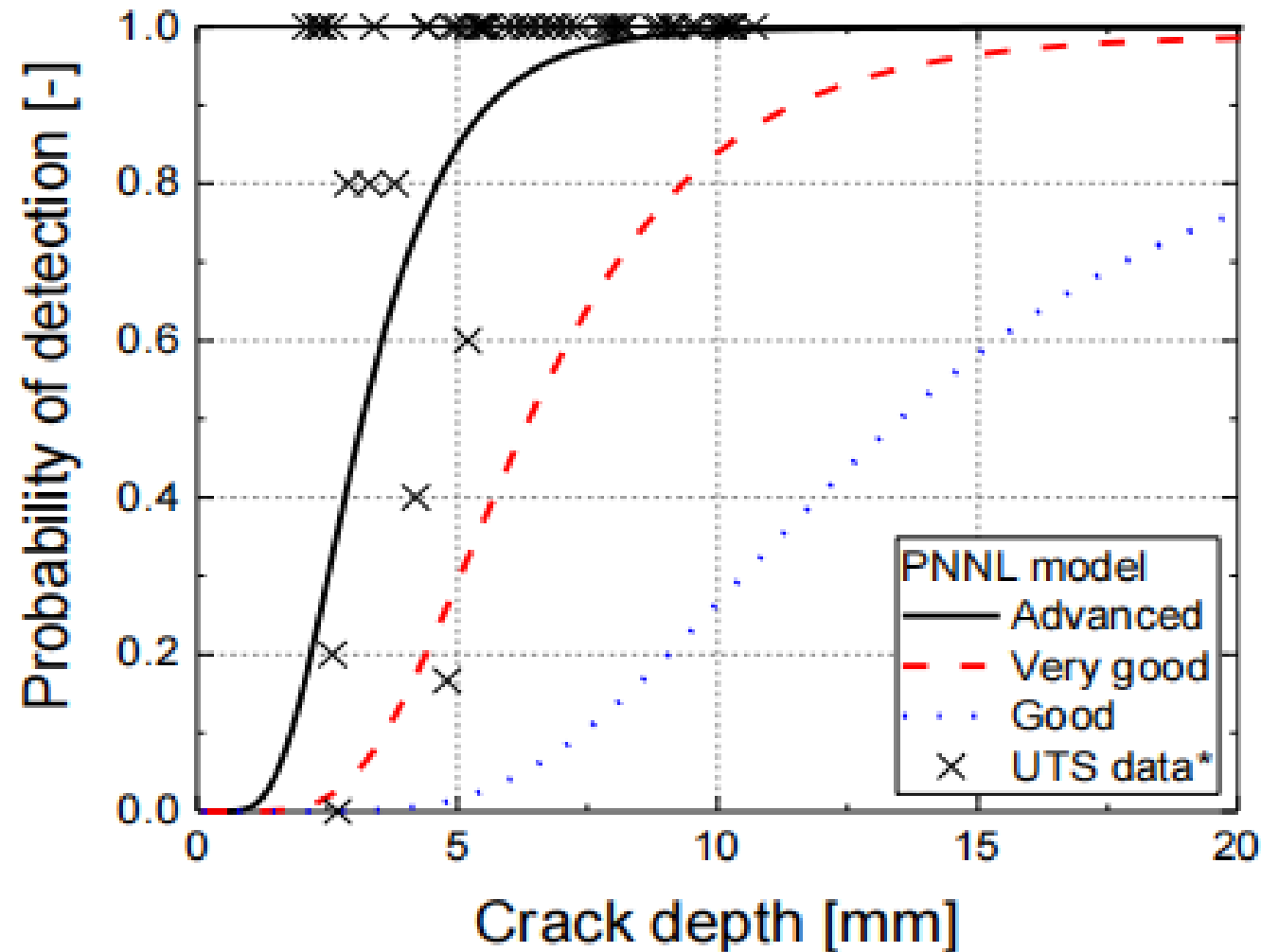
# Effect of Fatigue and Embrittlement on Through Wall Crack Frequency (TWCF) without ISI



VFLAL Crack Distribution  
Conservative embedded crack (10 mm)  
Realistic embedded crack (4.8 mm)

**Fatigue (---) does not affect the TWCF**  
→ "Justification 1" was not valid

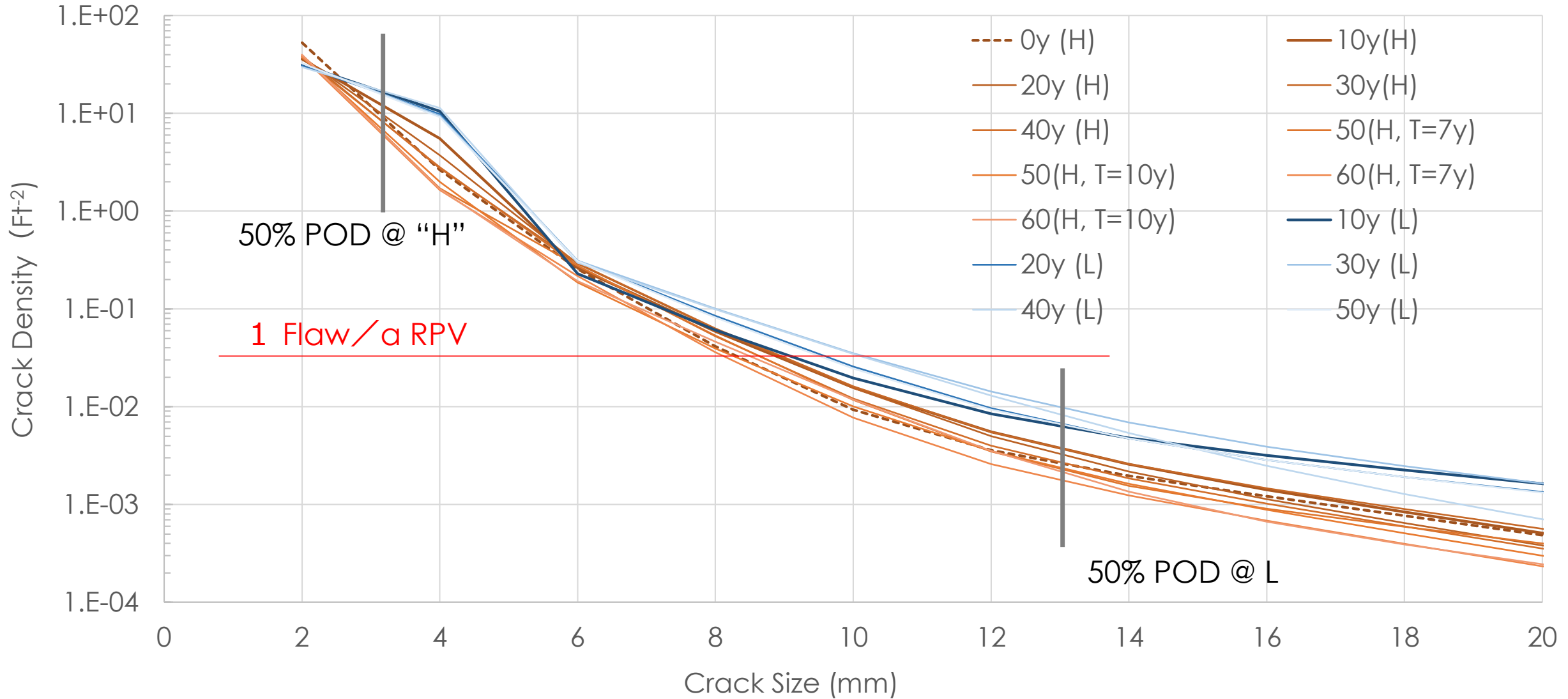
# Bayesian Update of Crack Distribution 亀裂分布の ベイズ更新の方法



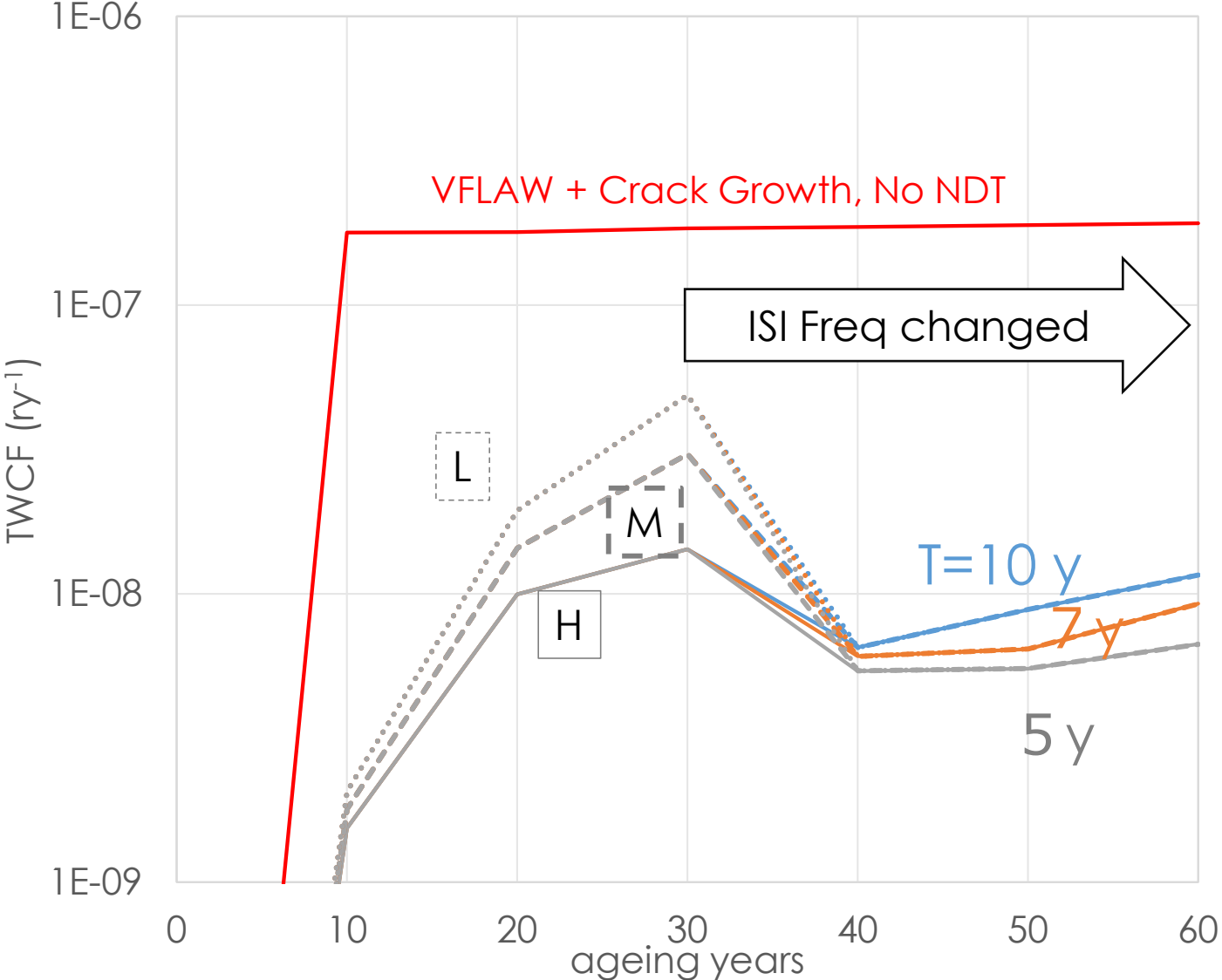
$$L(a|\Phi) = \frac{f(a|\Phi, t_{tr}) \cdot \text{POD}(a)}{\text{POD}(\Phi, t_{tr})}$$

Katsuyama, Proc. ASME PVP 2020

# Change in Crack Distribution at Weld line



# Change in TWCF by ISI



ISI reduces TWCF (one order)

→ "Justification 2" may be valid

POD does not affect TWCF during LTO?

# Conclusion

- ISI reinforcements in Japan would affect the structural integrity of the PWR as follows:
  1. On the beltline, **effect of fatigue is ignorable**, and crack distribution will not change significantly by the updating
  2. **Slight reduction of TWCF** was recognized by the ISI, but it is the order of  **$10^{-8}$  /reactor year**. Reason of this trend is under the estimation.