



# Probabilistic RPV Integrity Assessment: Safety Margin Quantification and Integration of Thermal-Hydraulic Uncertainties

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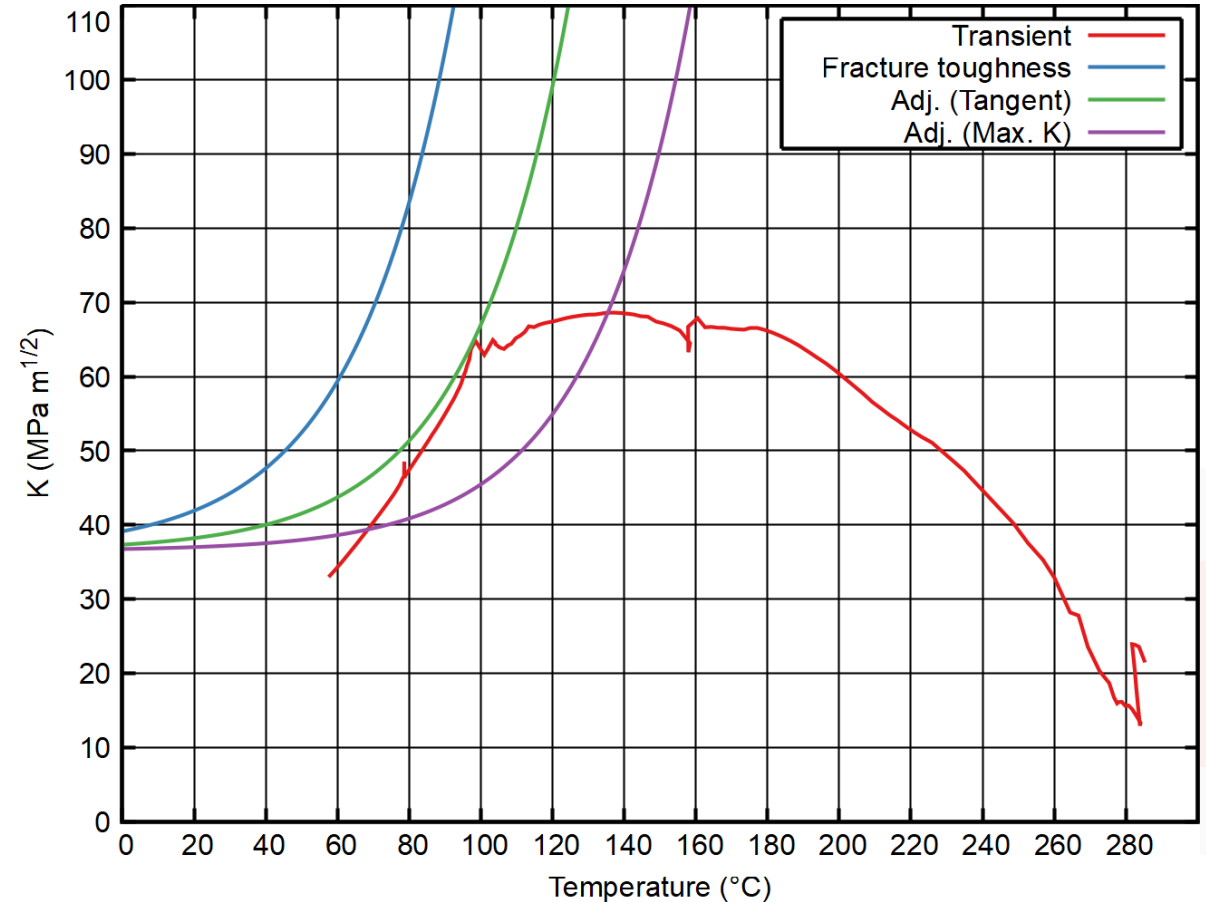


# Outline

- Introduction: Probabilistic RPV integrity assessment
- PART I: Probabilistic margin concepts
  - 3 concepts
  - Demonstration cases
  - Conclusions
- PART II: Thermal-Hydraulic Uncertainties
  - Probabilistic margin assessment including thermal-hydraulic uncertainties
  - Probabilistic assessment of set of transients
  - Vision of fully integrated assessment
- Final Summary

# Introduction: RPV integrity assessment

- RPV Integrity assessment
  - Pressurized thermal shock (PTS)
- Fracture-mechanics assessment
  - Crack postulate (TCC, UCC, EC)
  - Fracture toughness curve
- Deterministic margin
  - Maximal allowable adjusted reference temperature (Max. all. ART)
  - Depends on initiation criterion
    - Tangent
    - Max. K WPS



# PART I: Probabilistic margin assessment using 3 different concepts

# Introduction to probabilistic margin concepts

## Probabilistic margin concepts

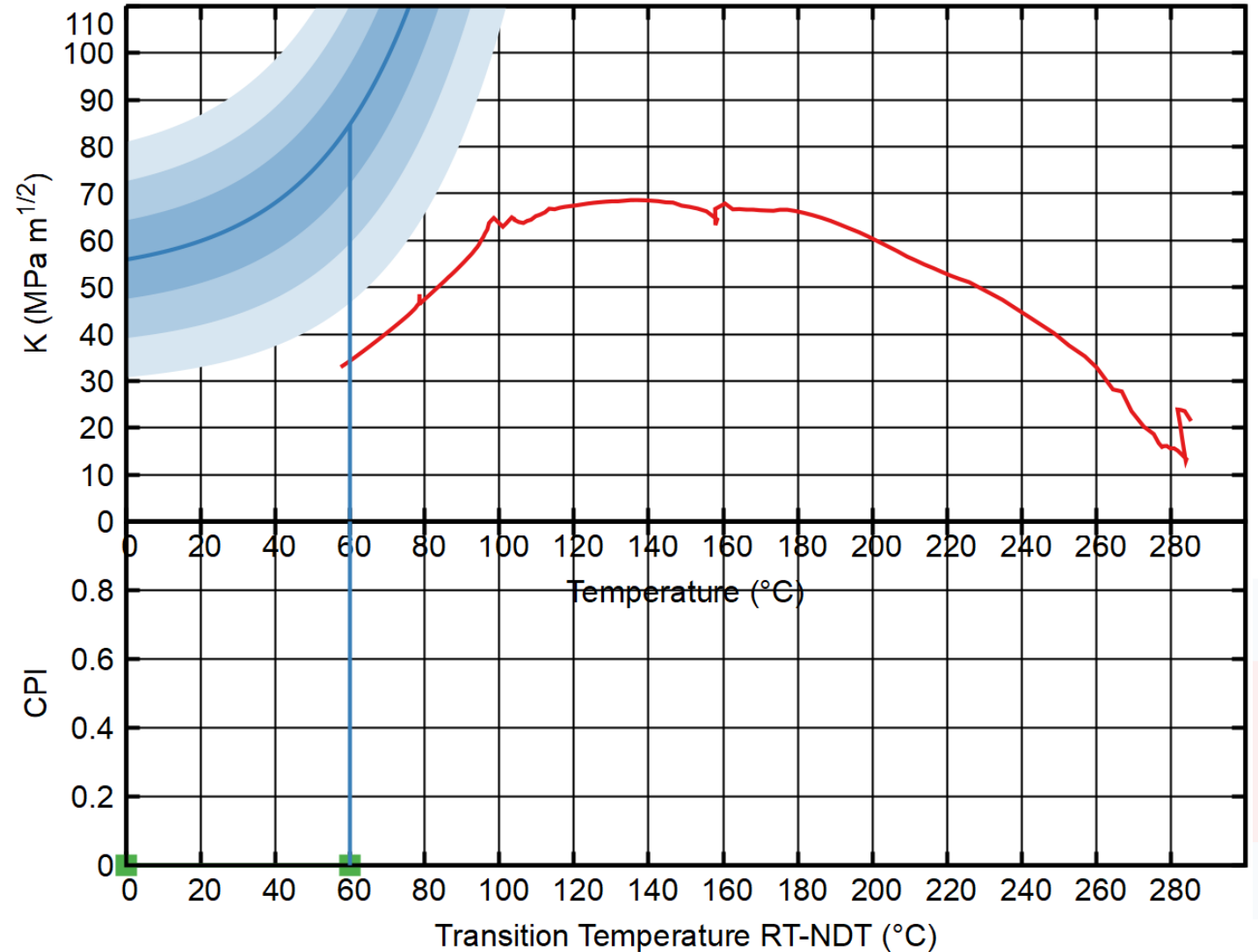
- i. Assessment based on maximal allowable adjusted reference temperature
- ii. Assessment based on lifetime
- iii. Assessment based on reliability theory

## Common background: Probabilistic acceptance criterion

- Marginally acceptable transient:
  - Conditional probability of initiation  $2.28e-4$

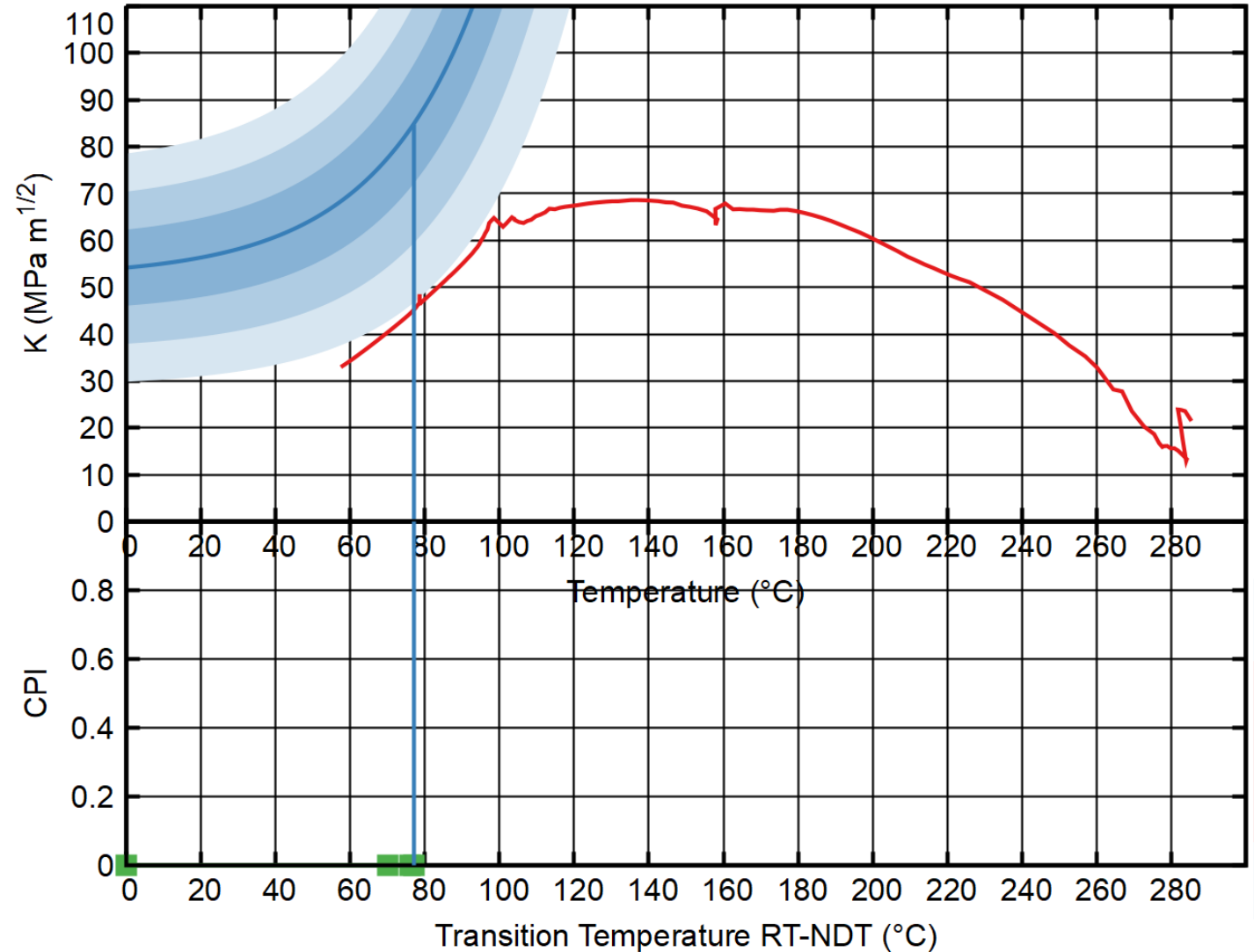
# Max. all. ART

- Distribution of fracture toughness
  - ASME-Curve: truncated normal distribution
- CPI depends on RT\_NDT
- Adjust transition temperature RT-NDT
- Find intersection point with target CPI
  - APAL-specific target for this type of transient:  $2.28 \times 10^{-4}$



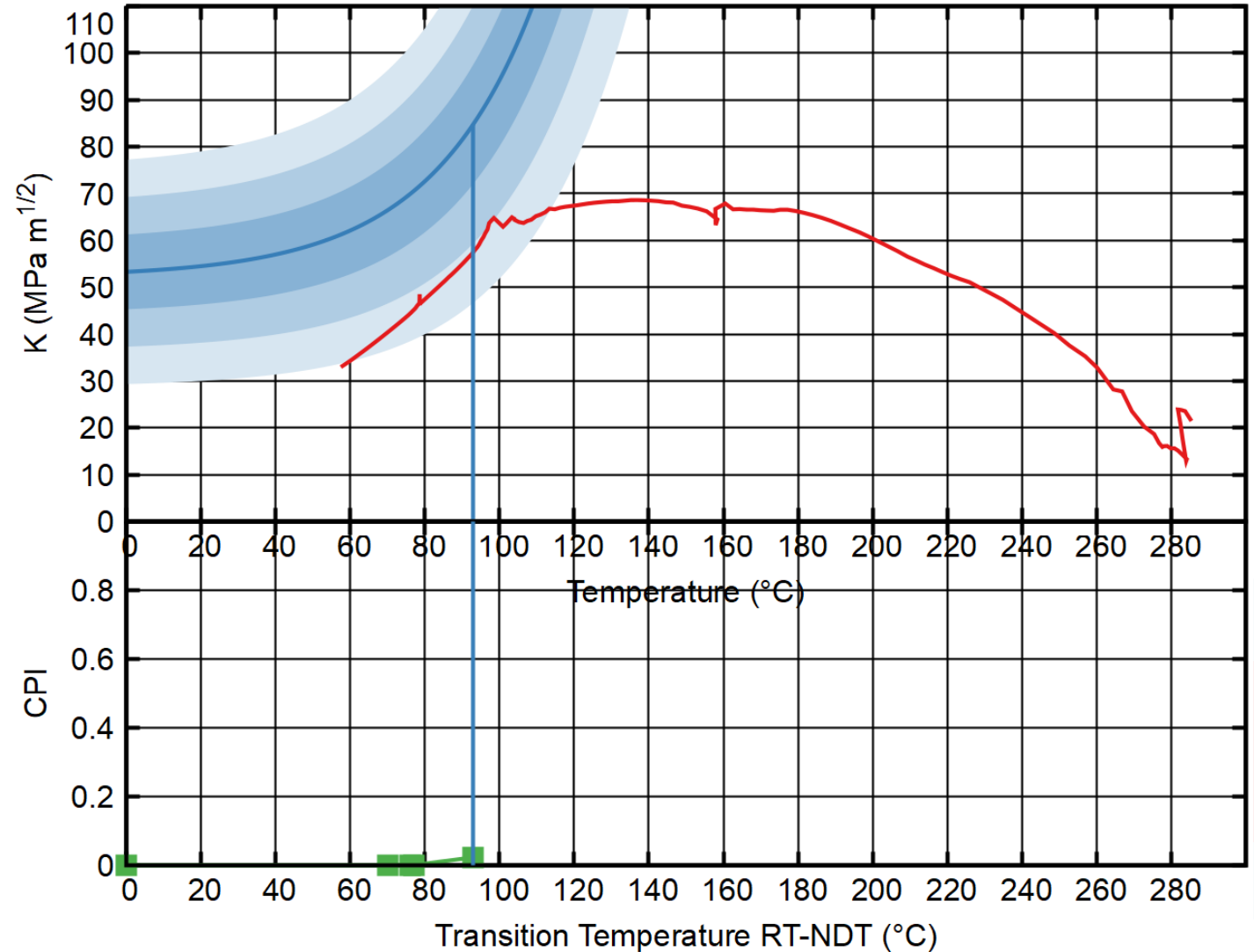
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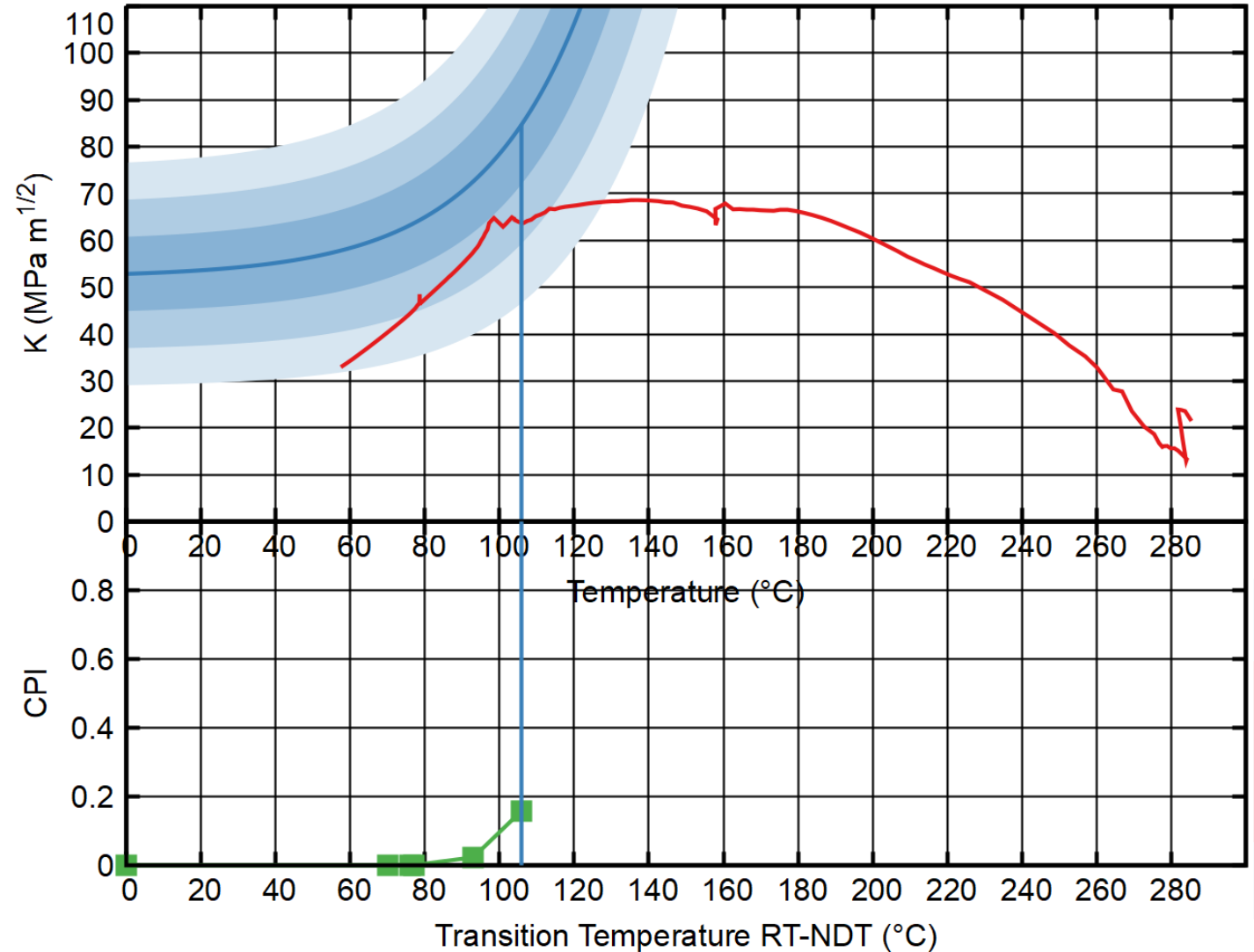
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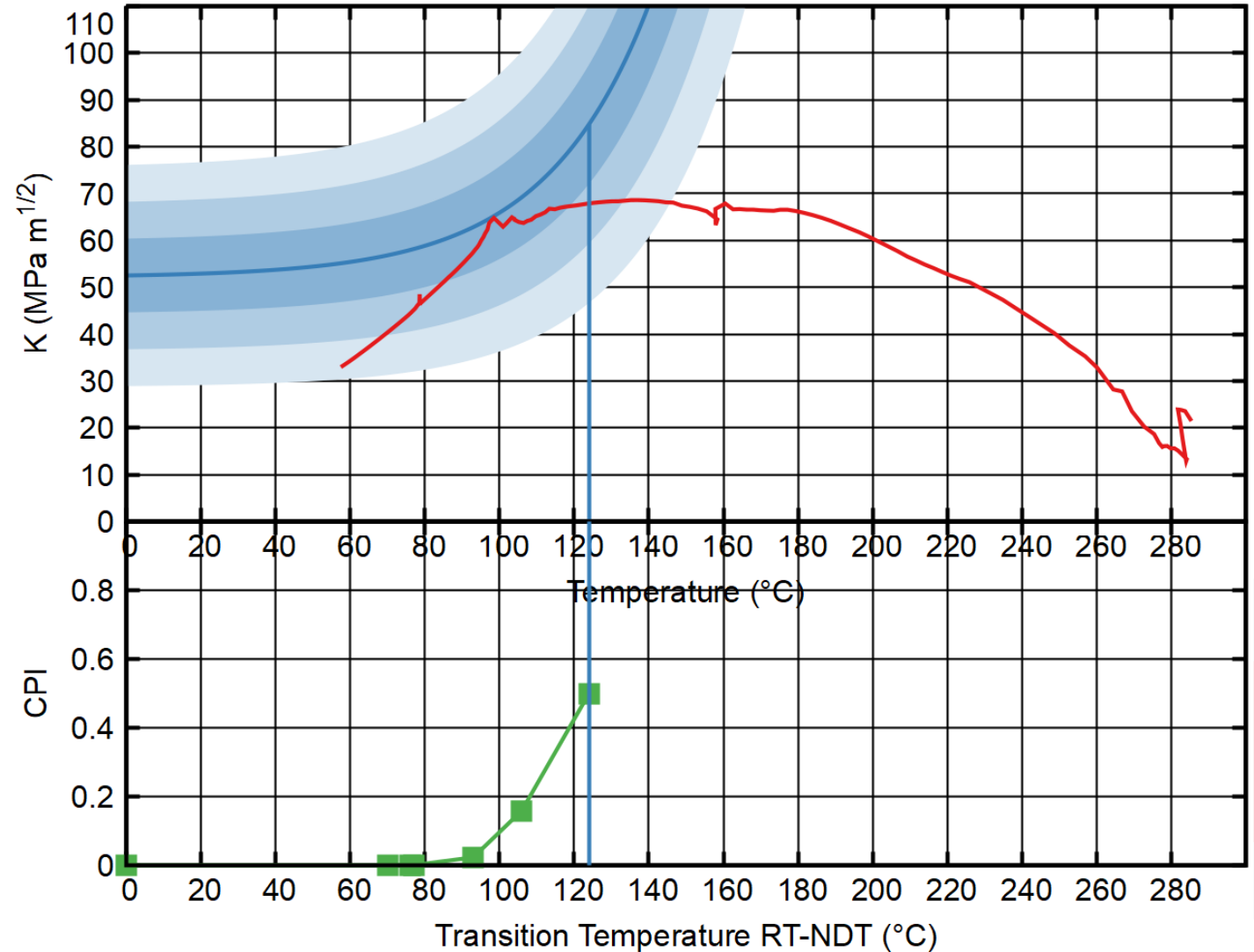
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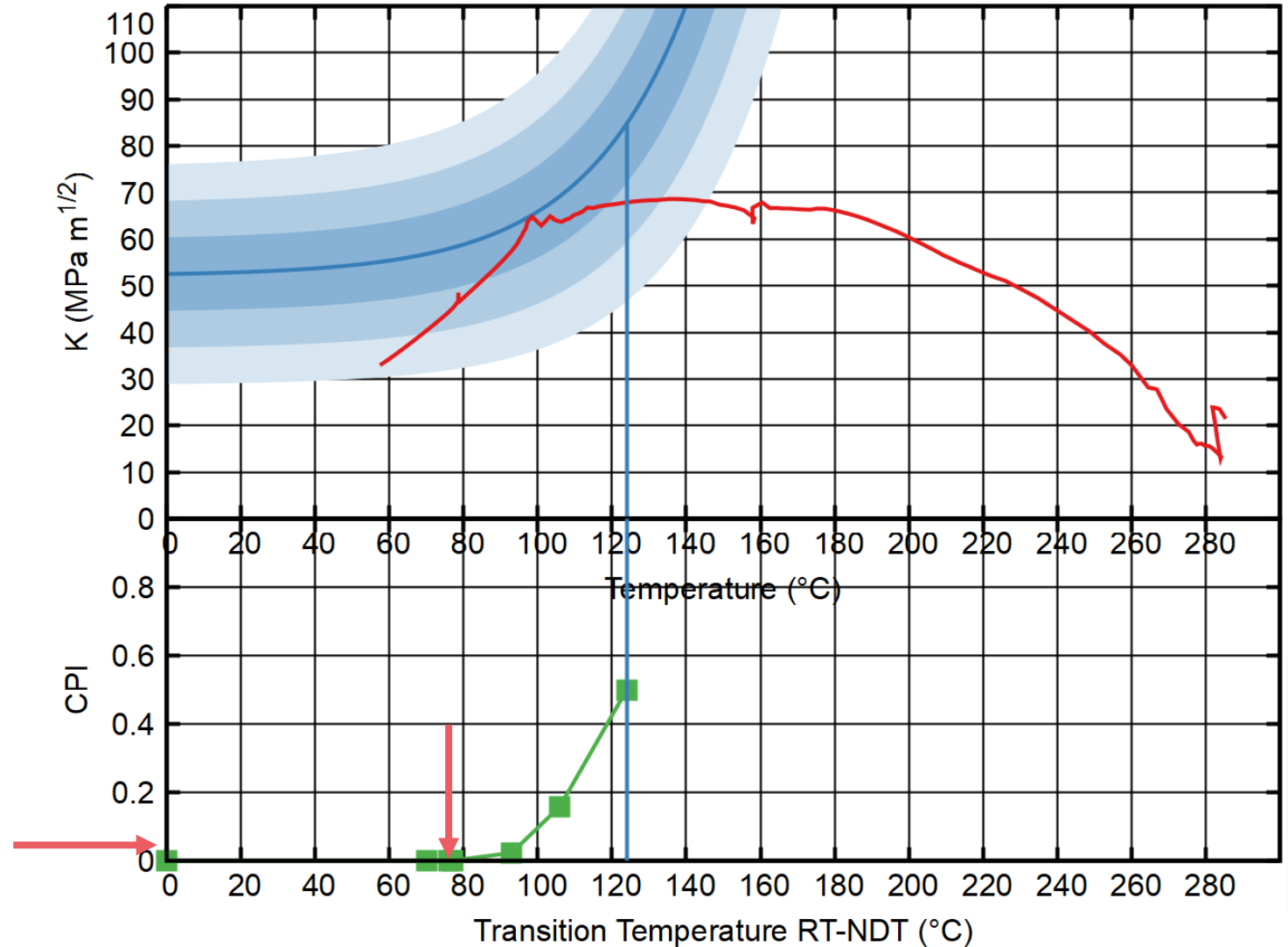
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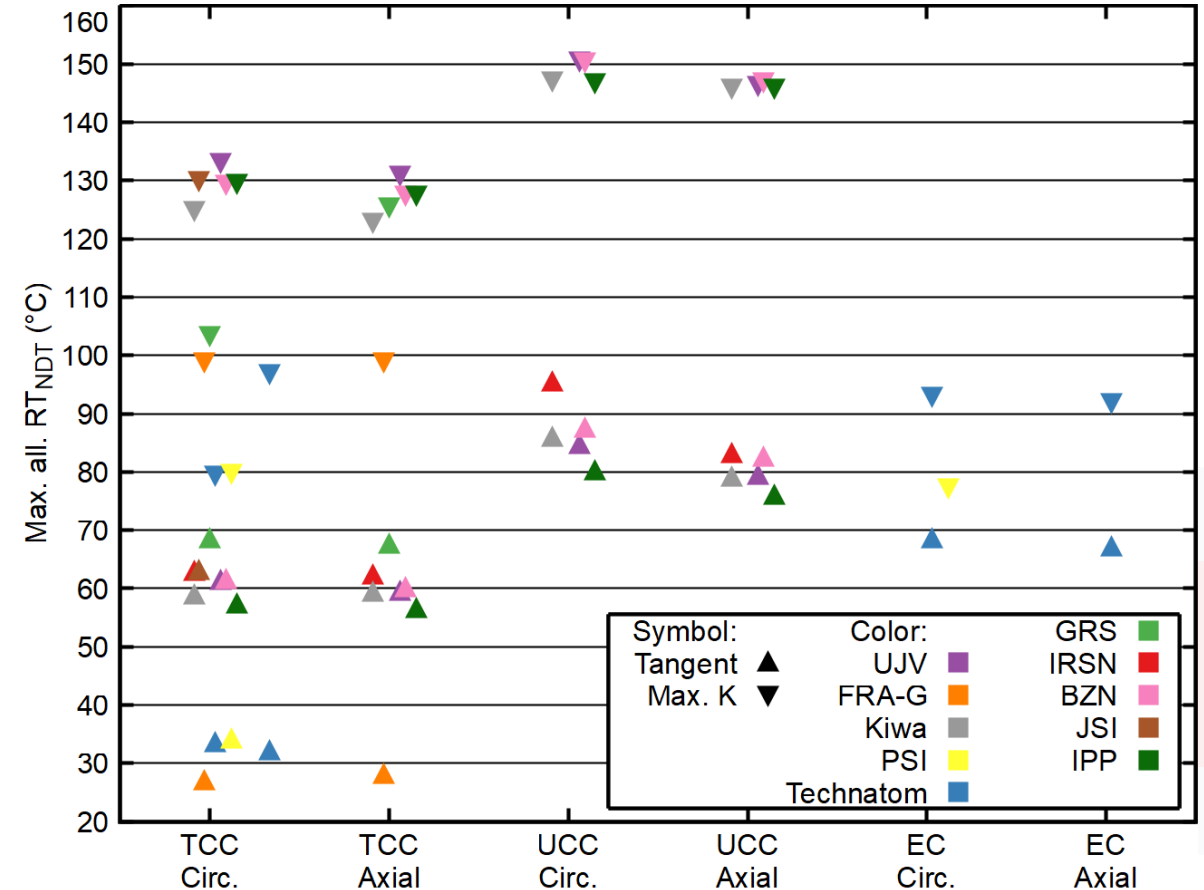
# Max. all. ART

- Distribution of fracture toughness
  - ASME-Curve: truncated normal distribution
- CPI depends on RT\_NDT
- Adjust transition temperature RT-NDT
- Find intersection point with target CPI: **77°C**
  - APAL-specific target for this type of transient:  $2.28 \times 10^{-4}$



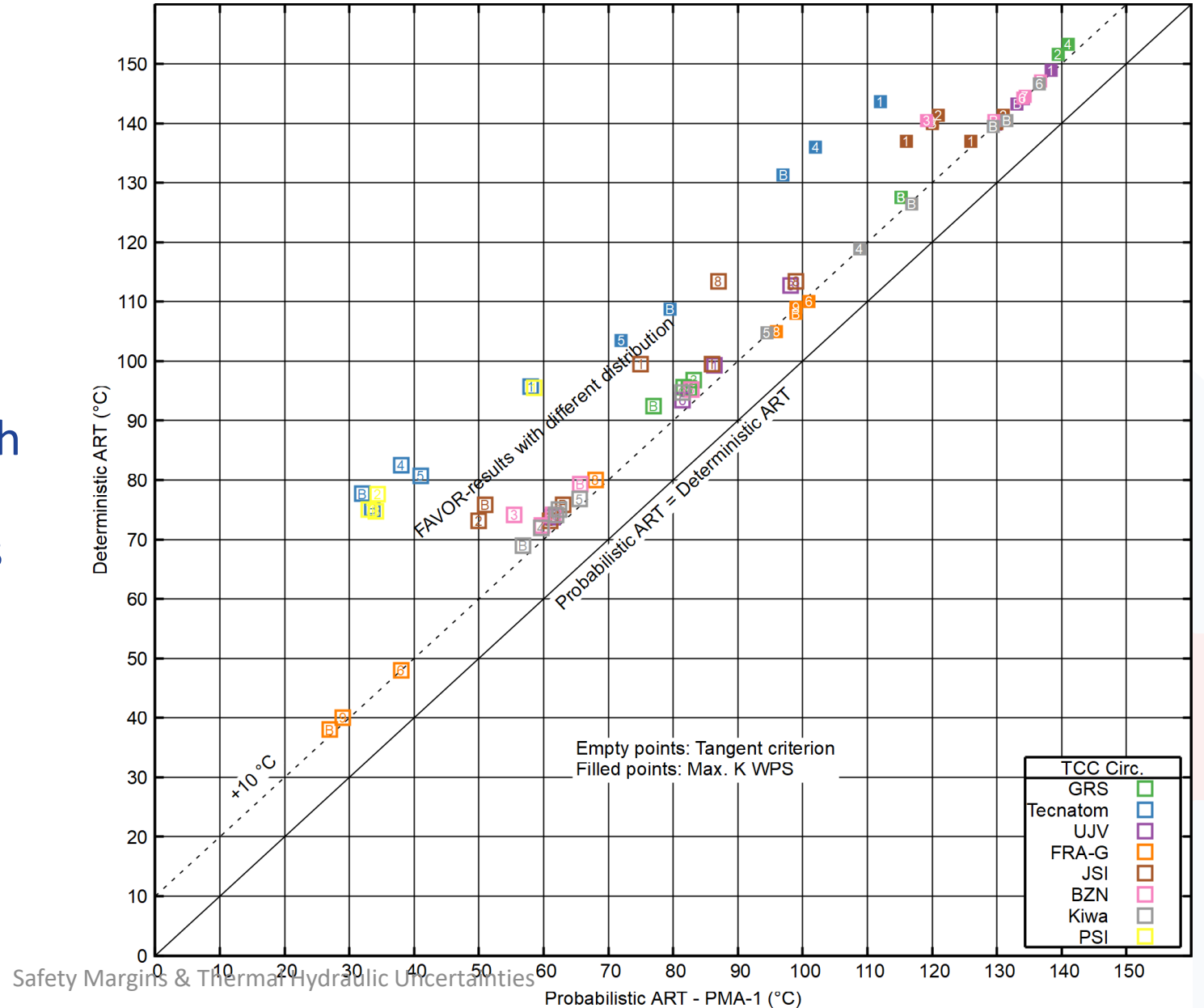
# Application cases

- „Baseline“ cases from APAL project
  - TCC, UCC; EC
  - Different TH system codes
  - Tangent vs. max. K WPS
- Agreement
  - TH code influence
  - Conservative trend for some participants
- Remark
  - Low max. all. ART with tangent crit.



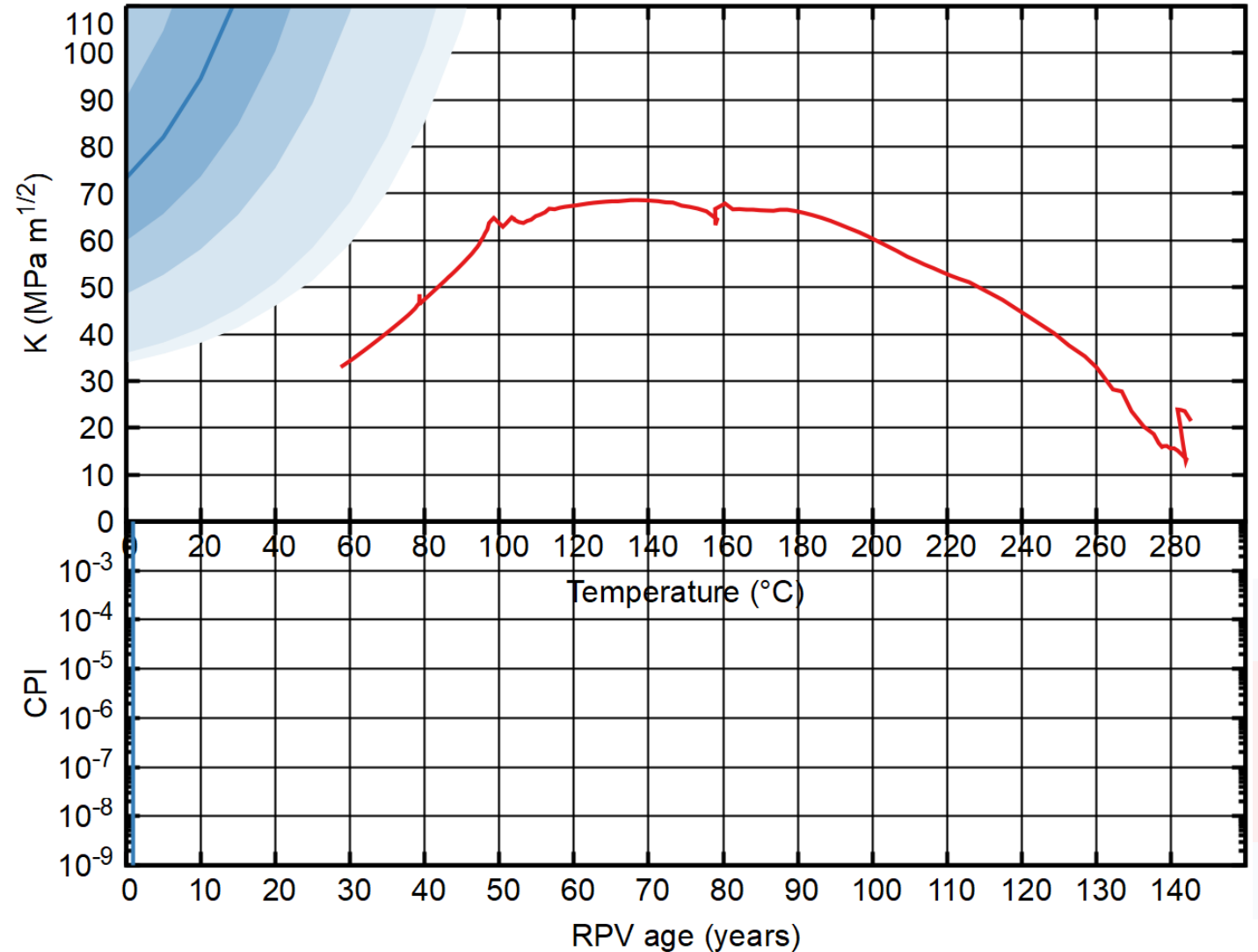
# Probabilistic vs. Deterministic margin

- Selection of different transients
- Simple relation
  - Exception: FAVOR users with Weibull distribution and different crack assumptions
- Trend note
  - Deterministic not envelope



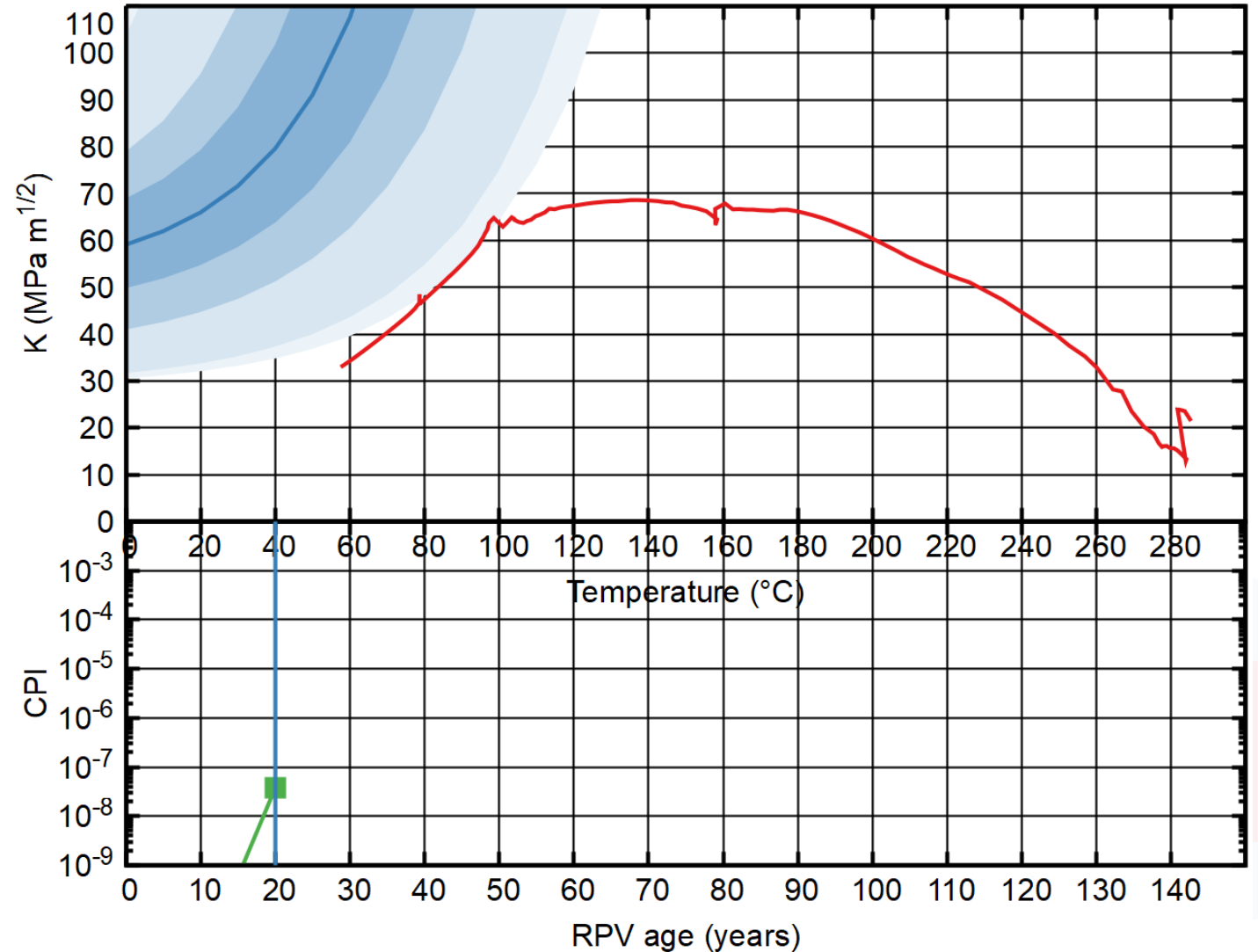
# Lifetime

- Distribution of fracture toughness
  - Fracture toughness level (as before)
  - Uncertainties in predicted RT-NDT
    - Due to chemistry, fluence, initial conditions
- Fluence depends on lifetime
  - Right-shift of fracture toughness
  - → CPI depends on lifetime
  - Find intersection point with target CPI



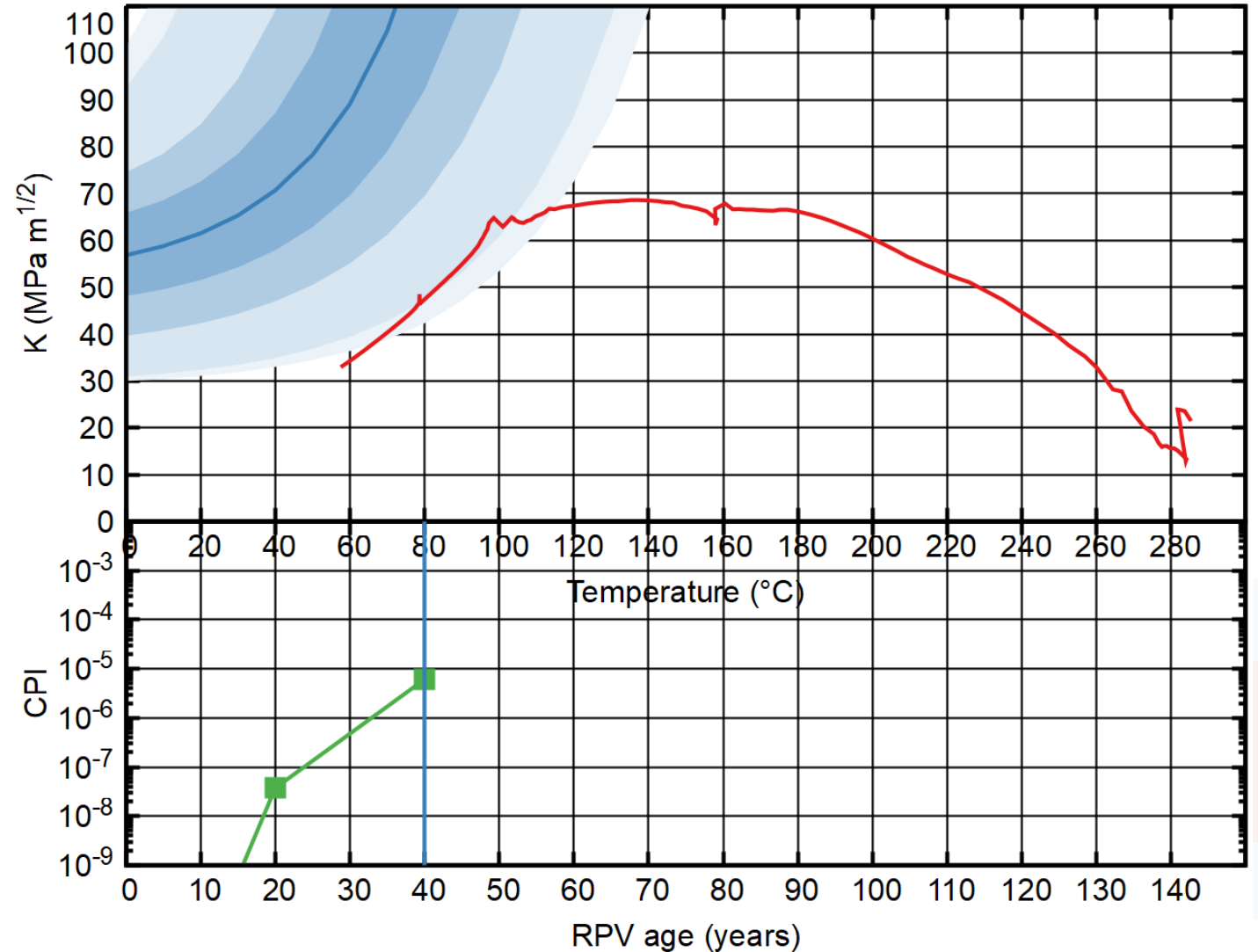
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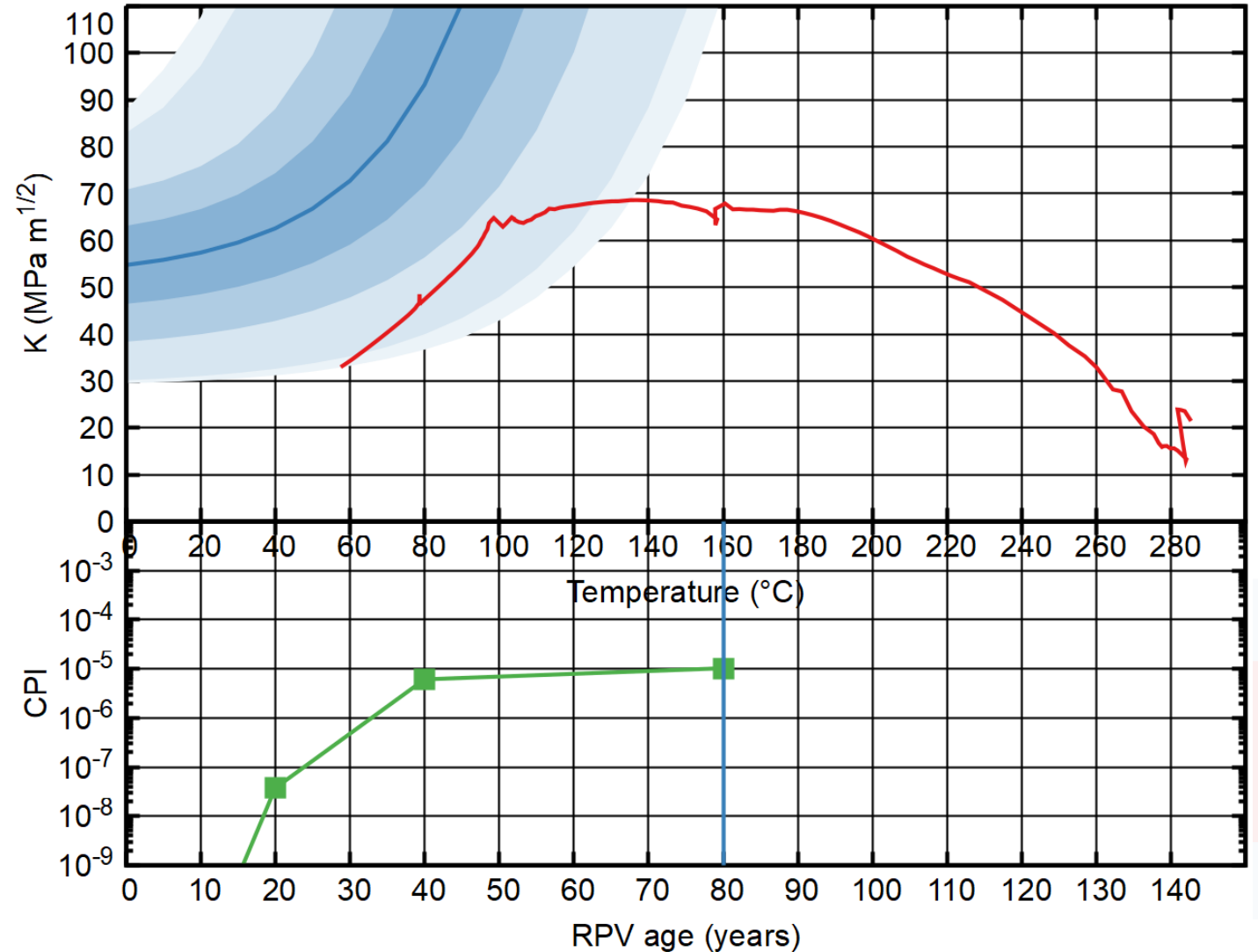
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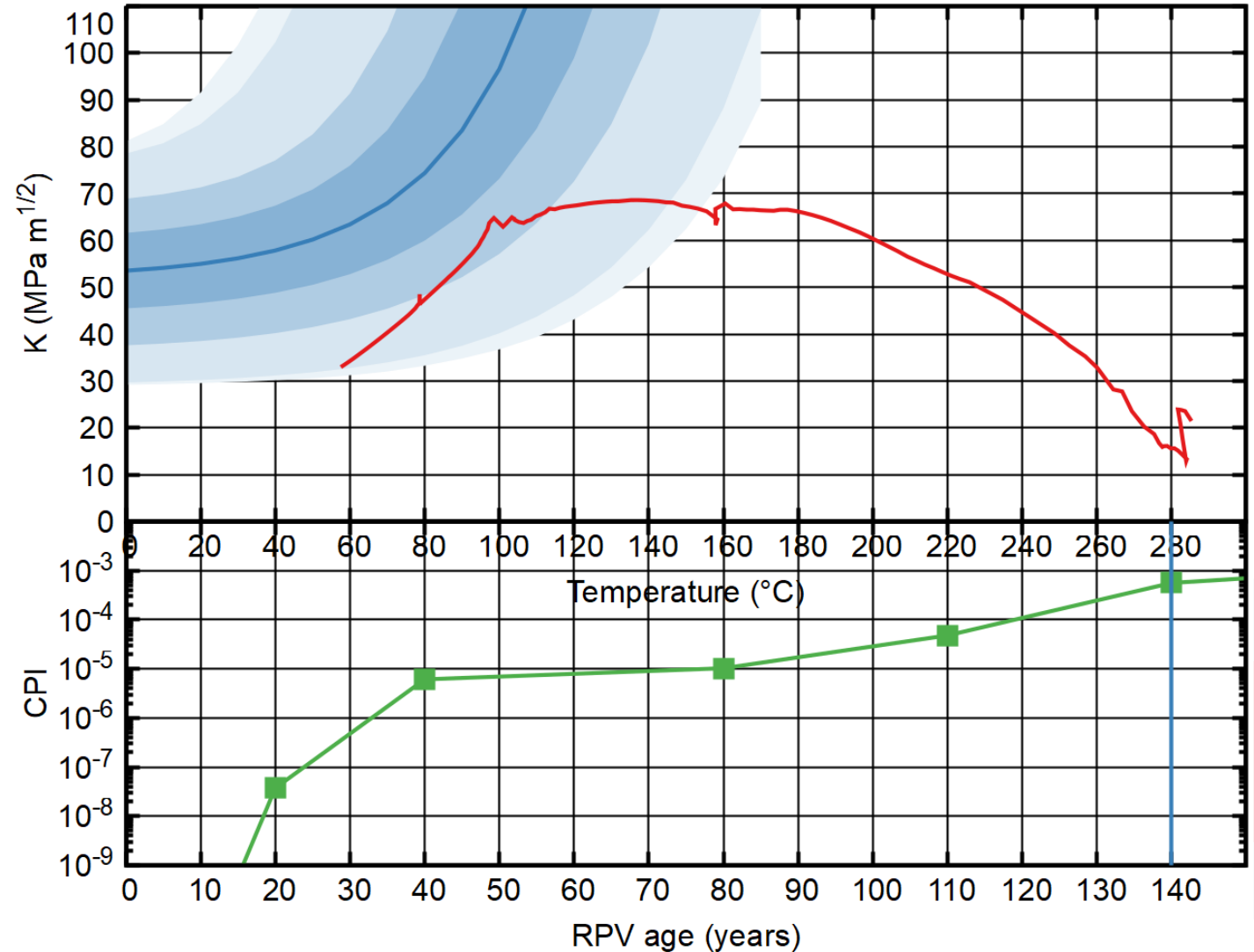
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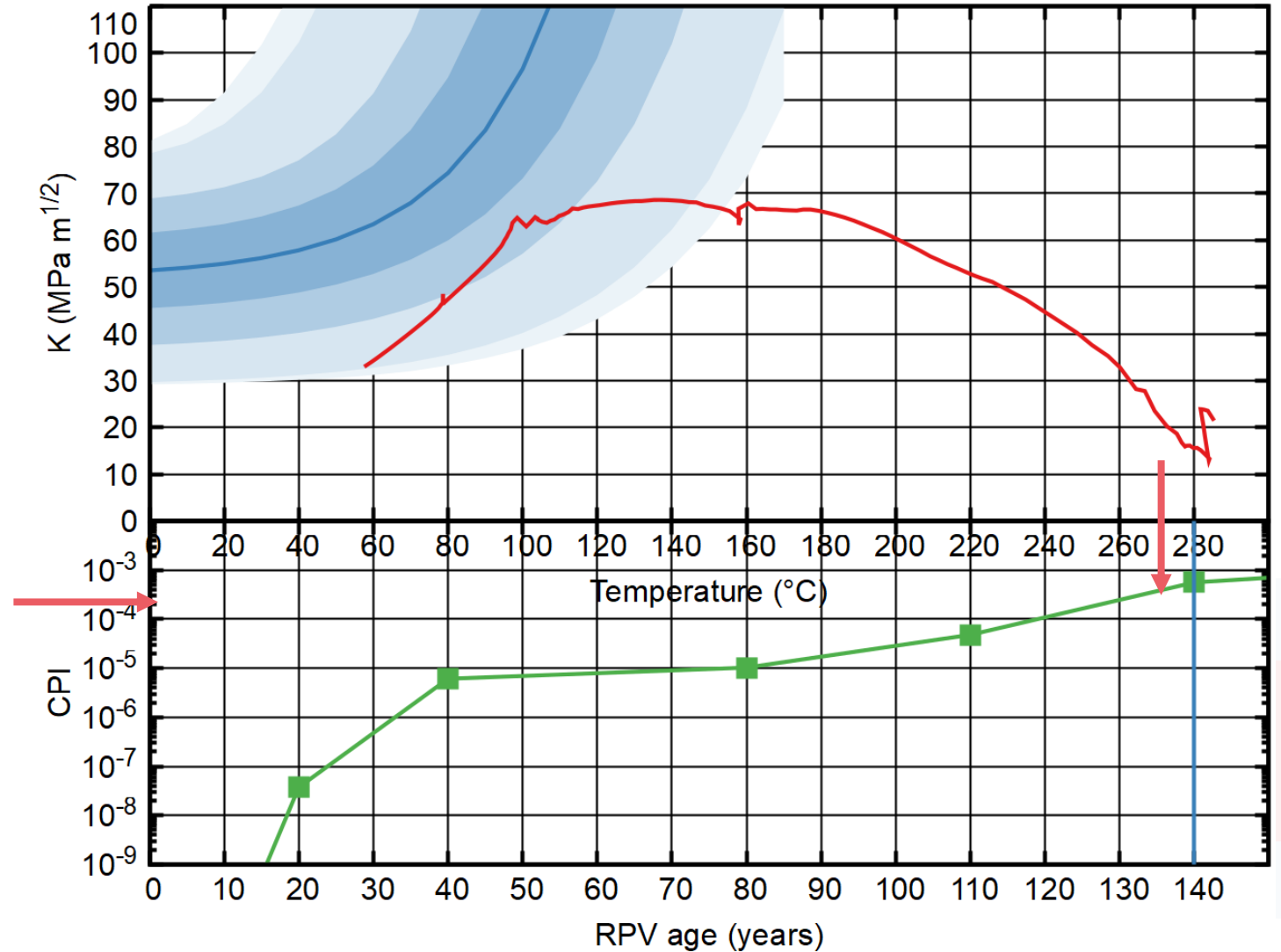
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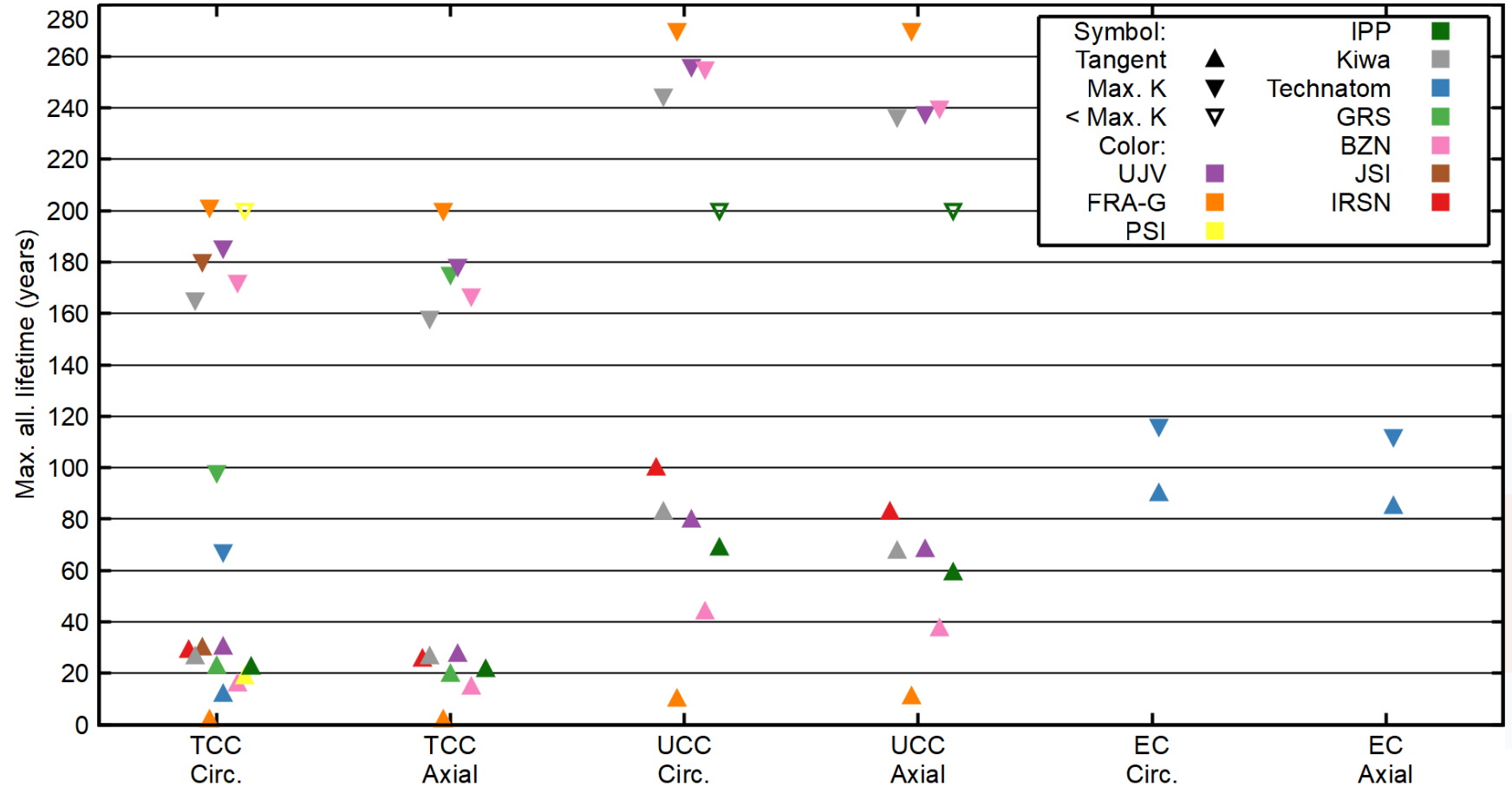
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  - Right-shift of fracture toughness
  - → CPI depends on lifetime
  - Find intersection point with target CPI: **~135 years**



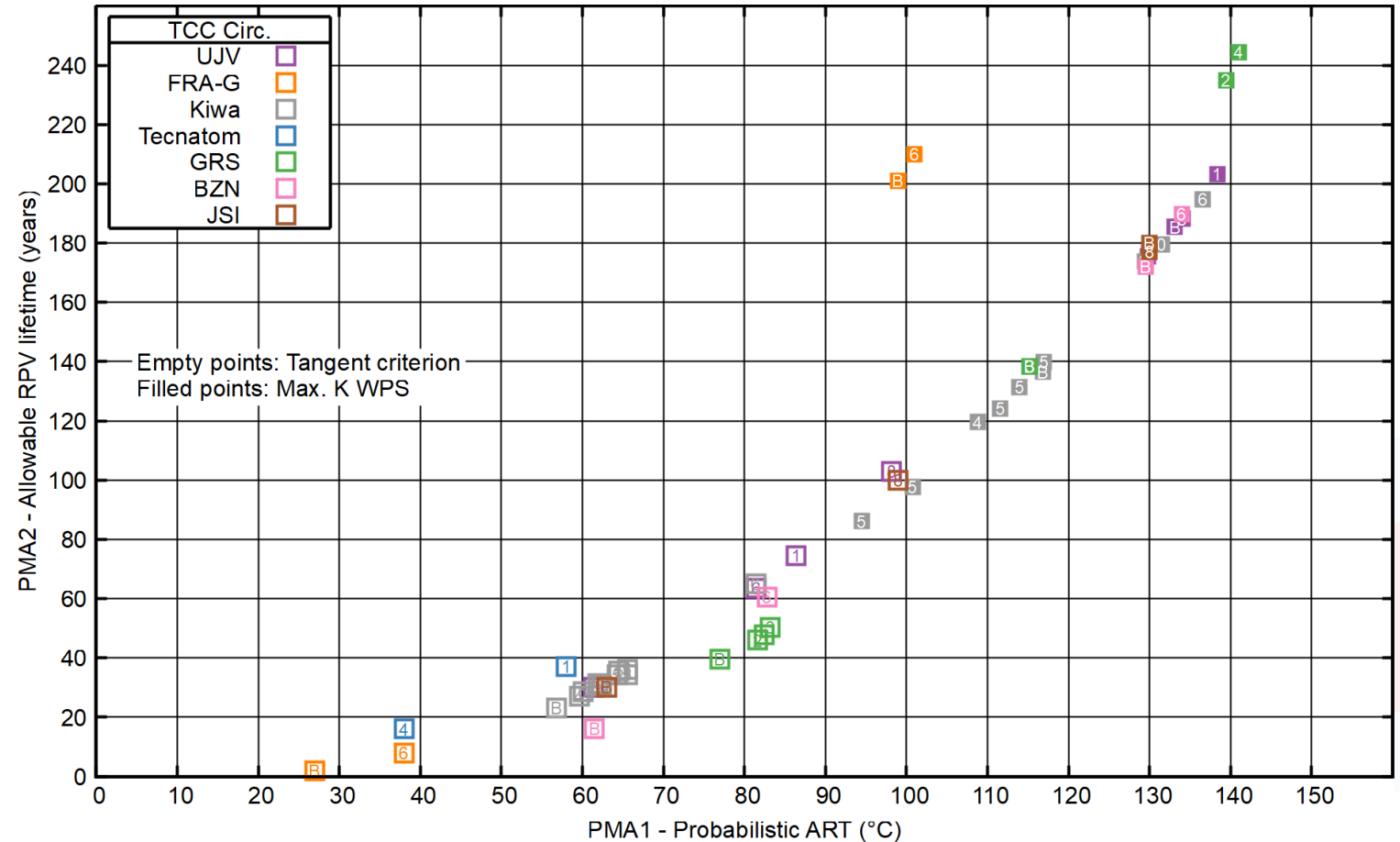
# Examples for lifetime margin

- Trends in agreement with max. all. ref. temperature
- Low allowable lifetime with tangent criterion
- High allowable lifetime with max. K WPS criterion



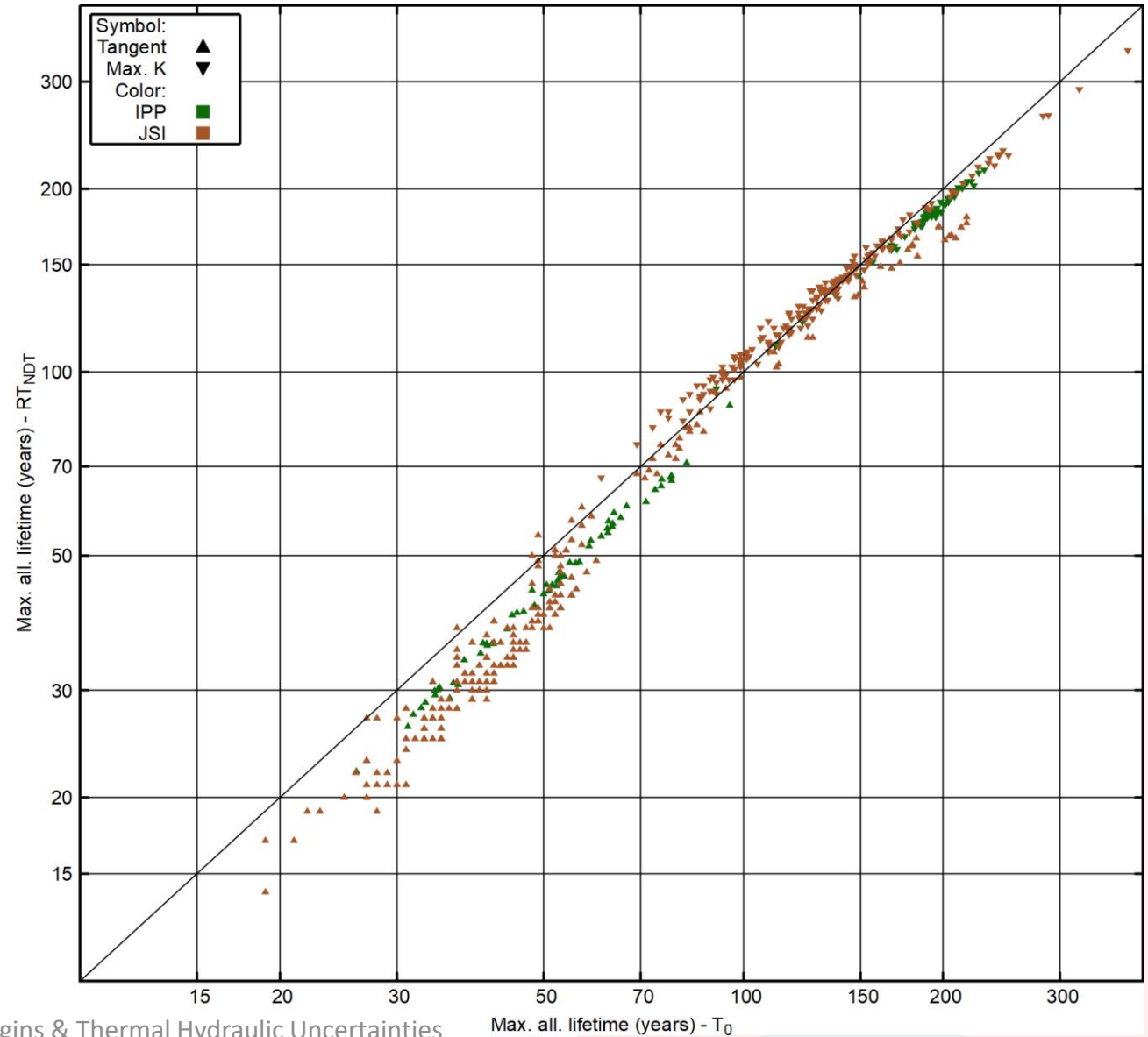
# Lifetime vs. max. all. ref. temperature

- Comparison of probabilistic margins
- Selection of different transients
- Result
  - Non-linear relation
  - Monotonic behavior
- Important for conclusion:
  - Different margin concepts lead to same ranking



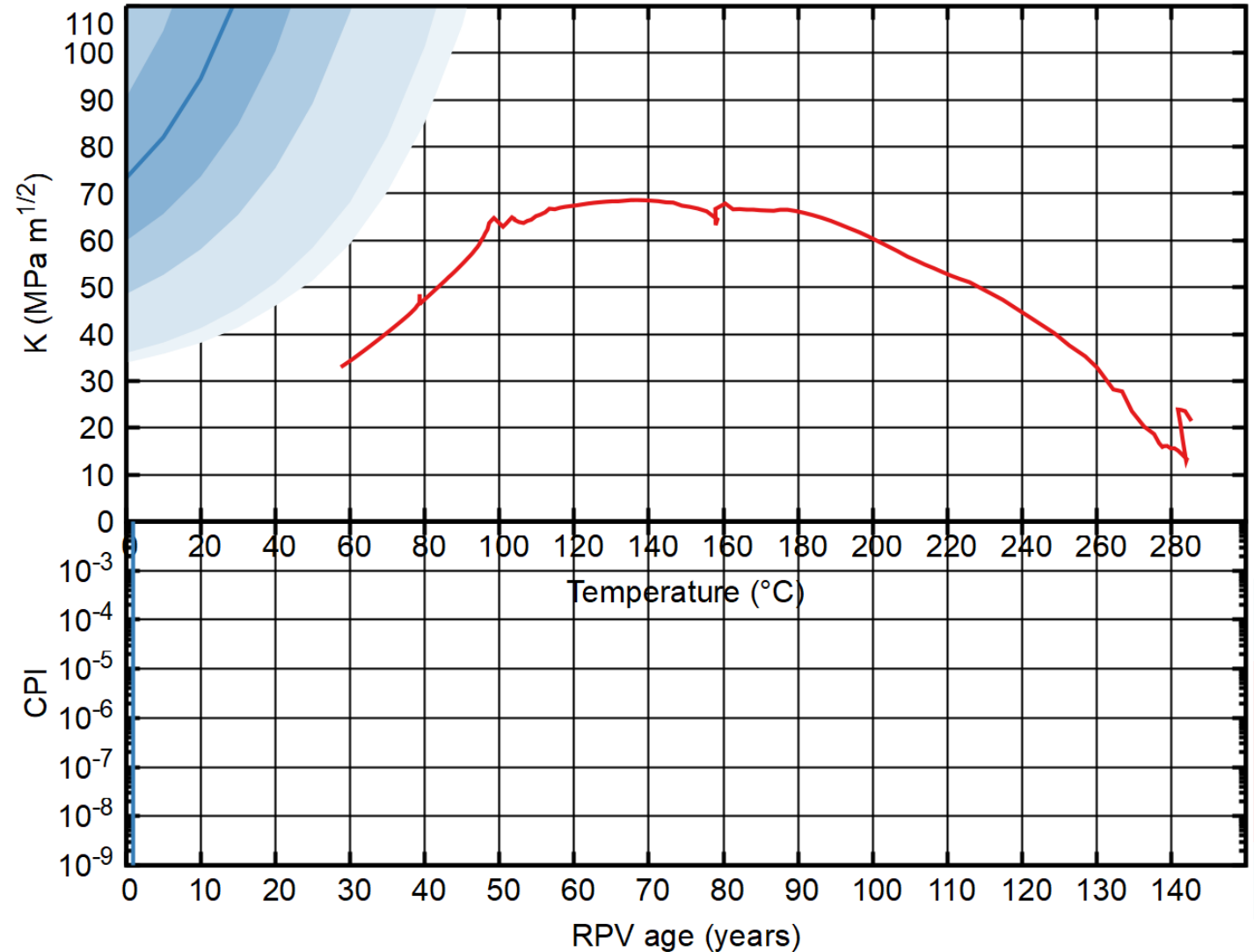
# Influence of fracture toughness curve

- Larger set of transients
- Compute lifetime with...
  - ASME curve
  - Master curve
- Dependence is implicate
  - Both enter in lifetime
- Slight differences



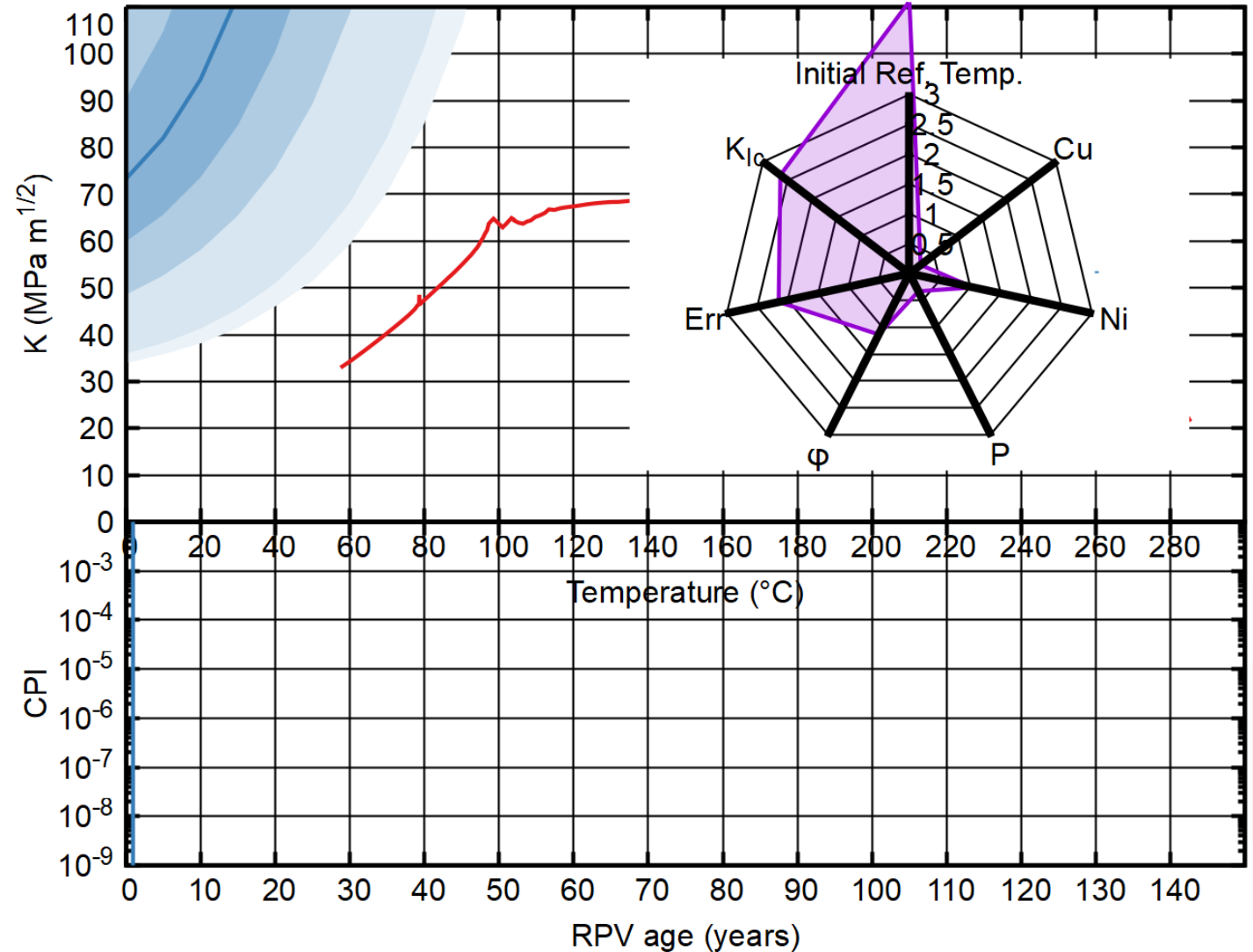
# Reliability and sensitivity

- Distribution of fracture toughness
  - 7 different parameters
- Limit state function and failure area
  - Visualization for 2 dimensions
- Transformation to std. normal space
- Most probable failure point (MPFP)
- Importance factors
  - $|MPFP_i|/\beta$
  - Ranking of relevant parameters



# Reliability and sensitivity

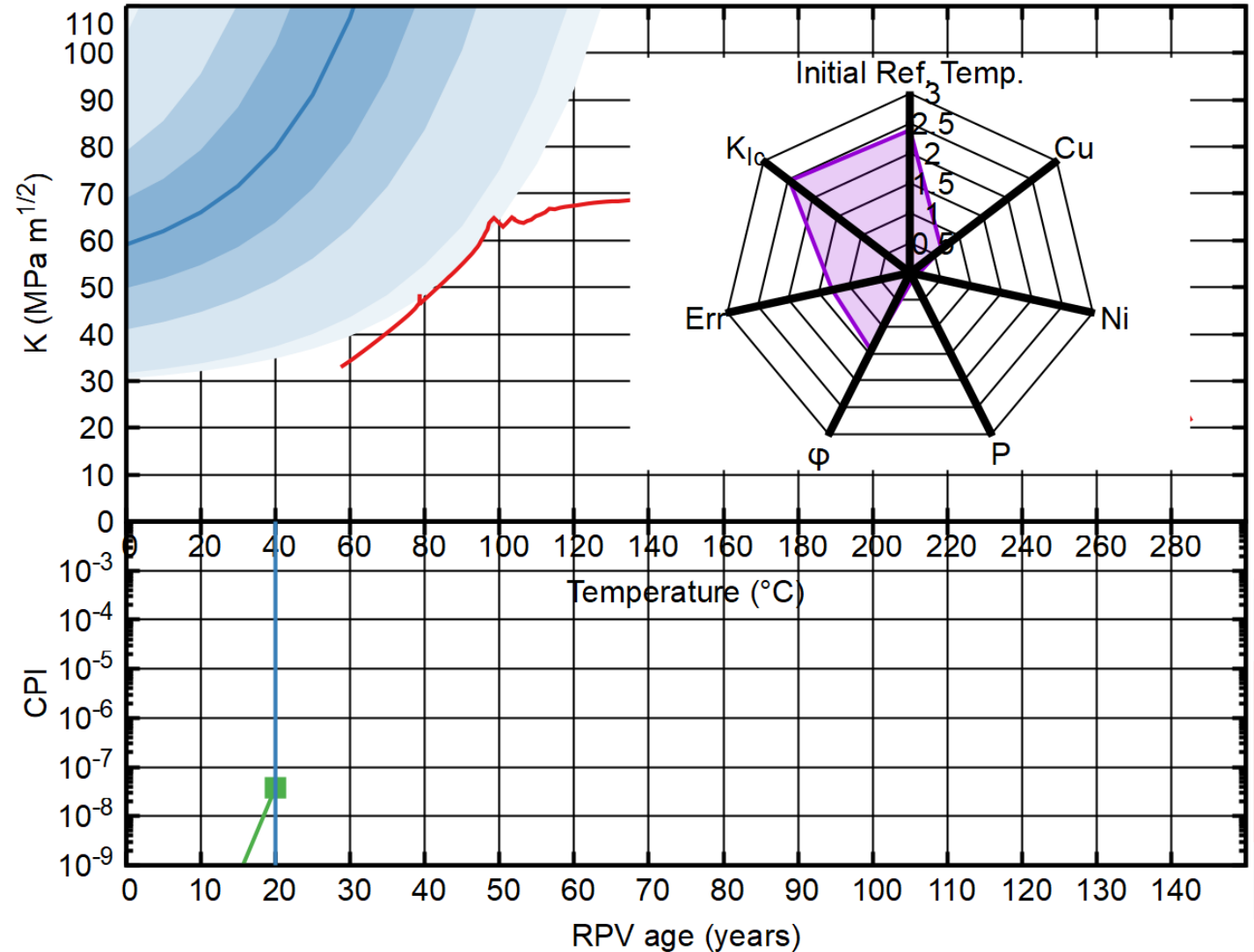
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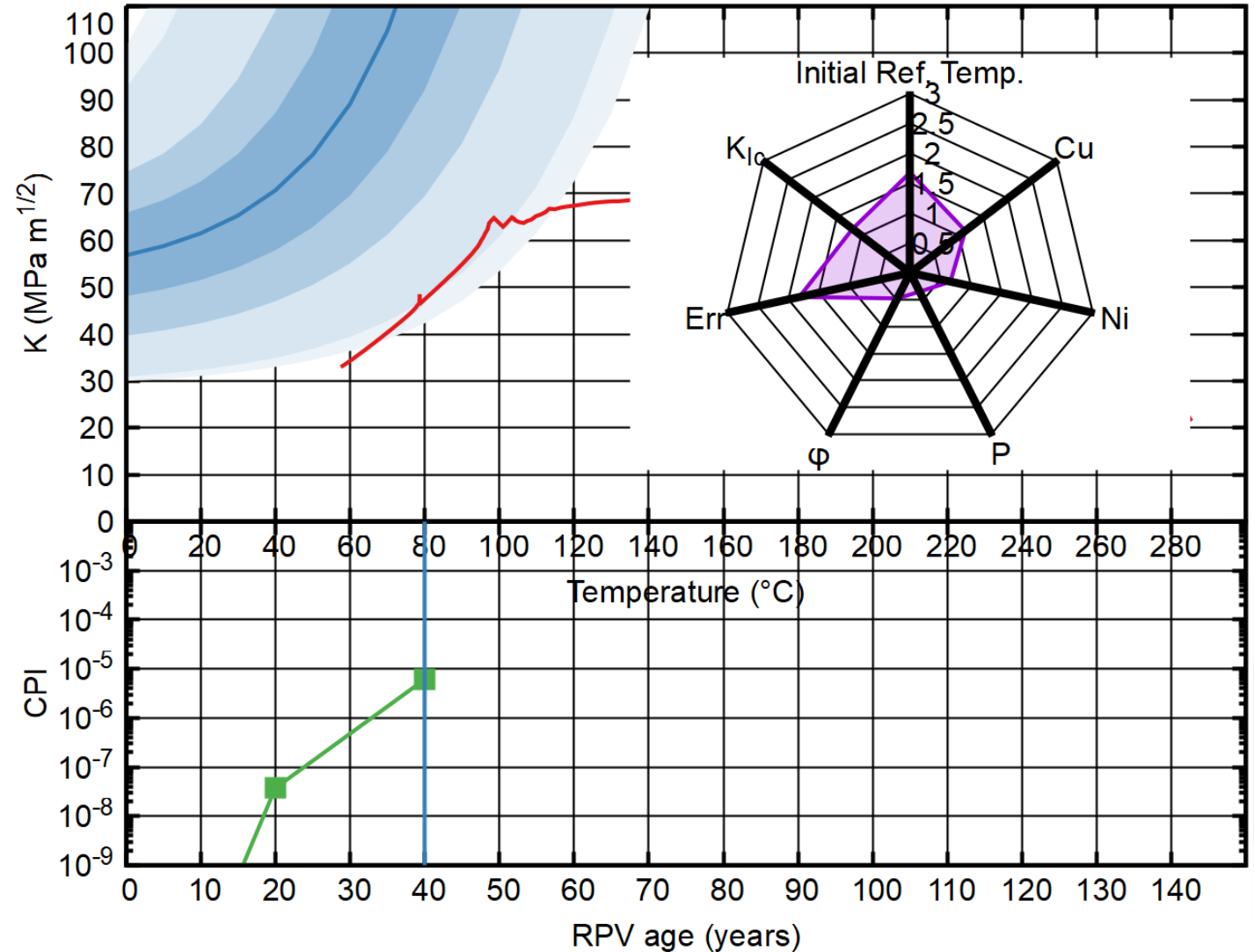
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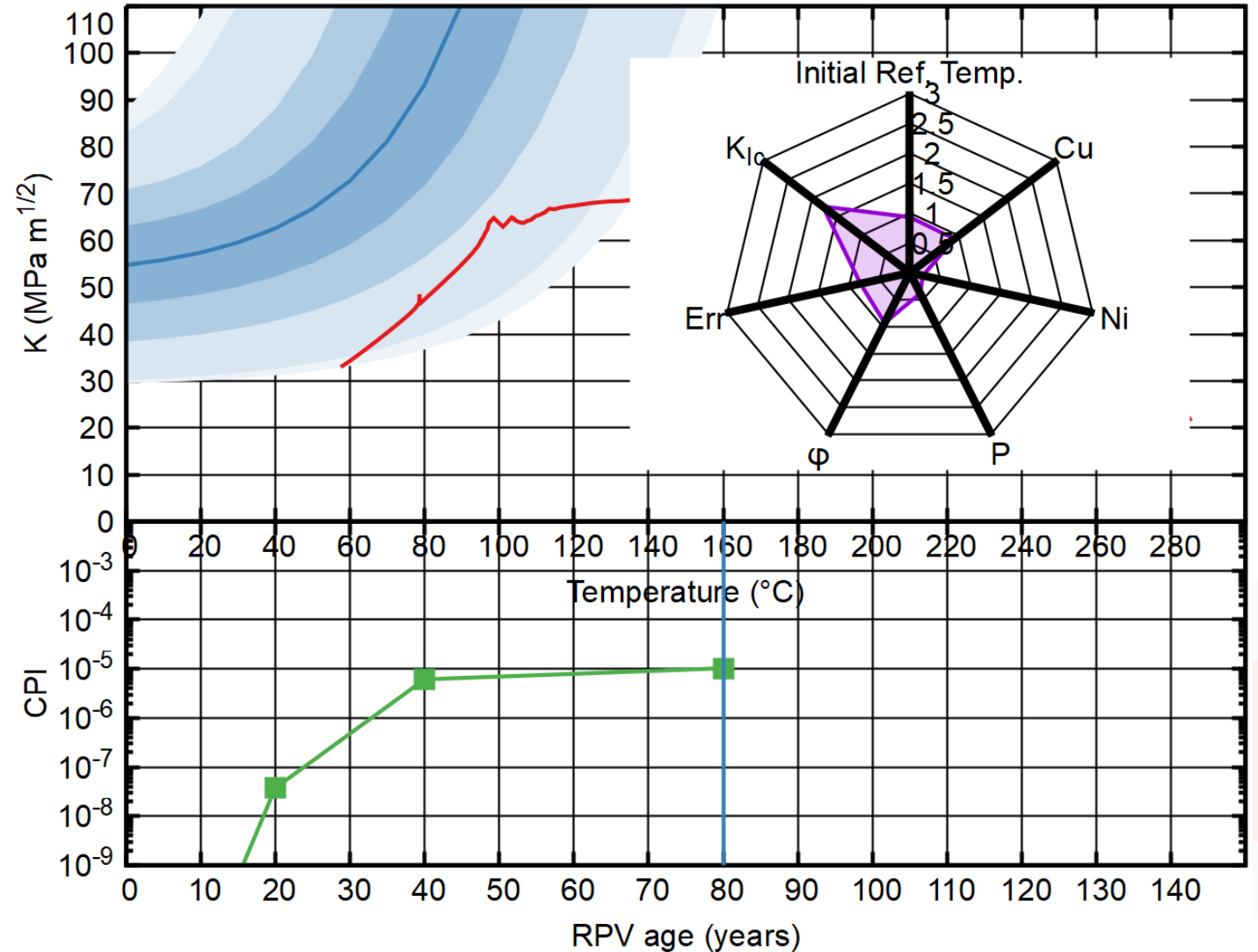
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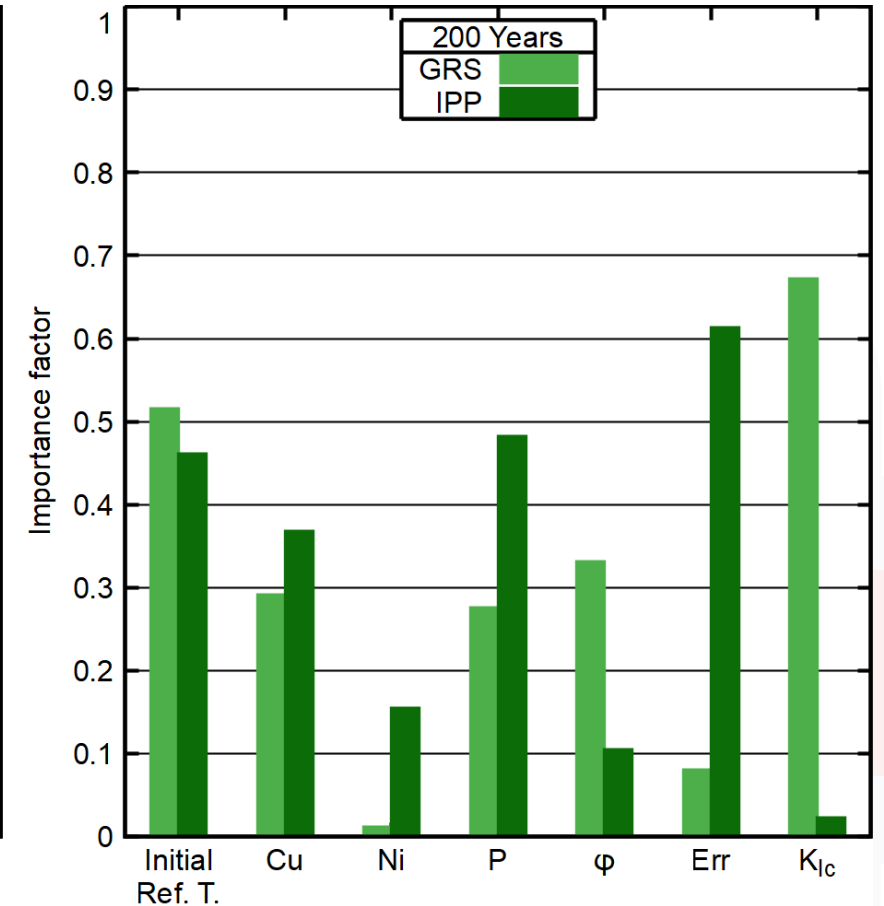
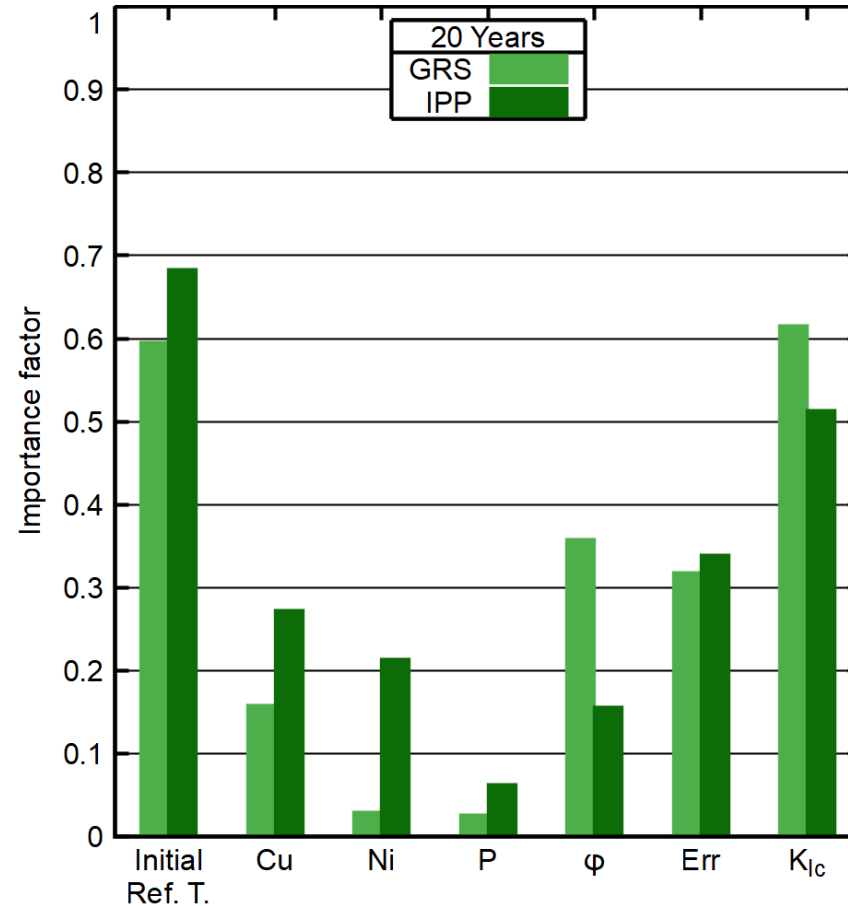
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# PMA-4: Importance factors

- Importance factors
  - $|MPFP_i|/\beta$
  - Ranking of relevant parameters
- Selected ages
  - 20 years
  - 200 years
- Agreement
  - For 20 years
  - Difference for 200 – but high probability



# Methodology conclusion

- **Fracture toughness margin**
  - Very limited additional information, compared to deterministic assessment
  - Remark: No crack size distribution was considered in the presented cases
  - Result would be less trivial for distributed crack size + fracture toughness based margin assessment
- **Lifetime margin**
  - Clear quantification of safety margin (lifetime)
  - Remark: Dependence on embrittlement model
- **Reliability and sensitivity margin**
  - Similar to PMA-2, understanding of mechanisms and risks
  - Generalization beyond initiation (i.e. crack arrest) open
- **Relation between margin approaches**
  - Monotonic relations (or even linear relations)
  - Consequence: Transients can be ranked/rated on deterministic level
    - (monotonic relation deterministic → fracture toughness → lifetime)

# PART II:

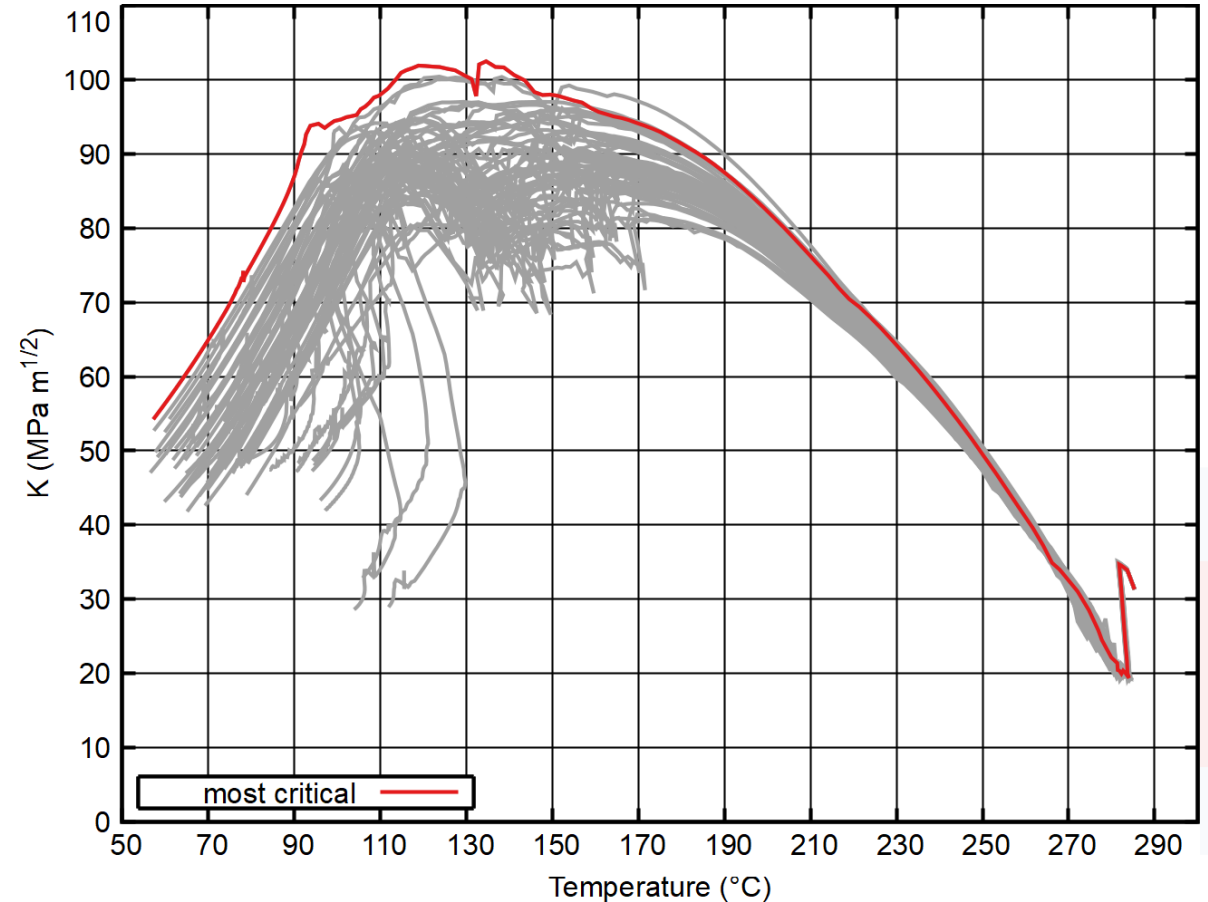
## Thermal-Hydraulic Uncertainties

and their inclusion in probabilistic margin assessment

# Thermal-hydraulic uncertainties: Introduction

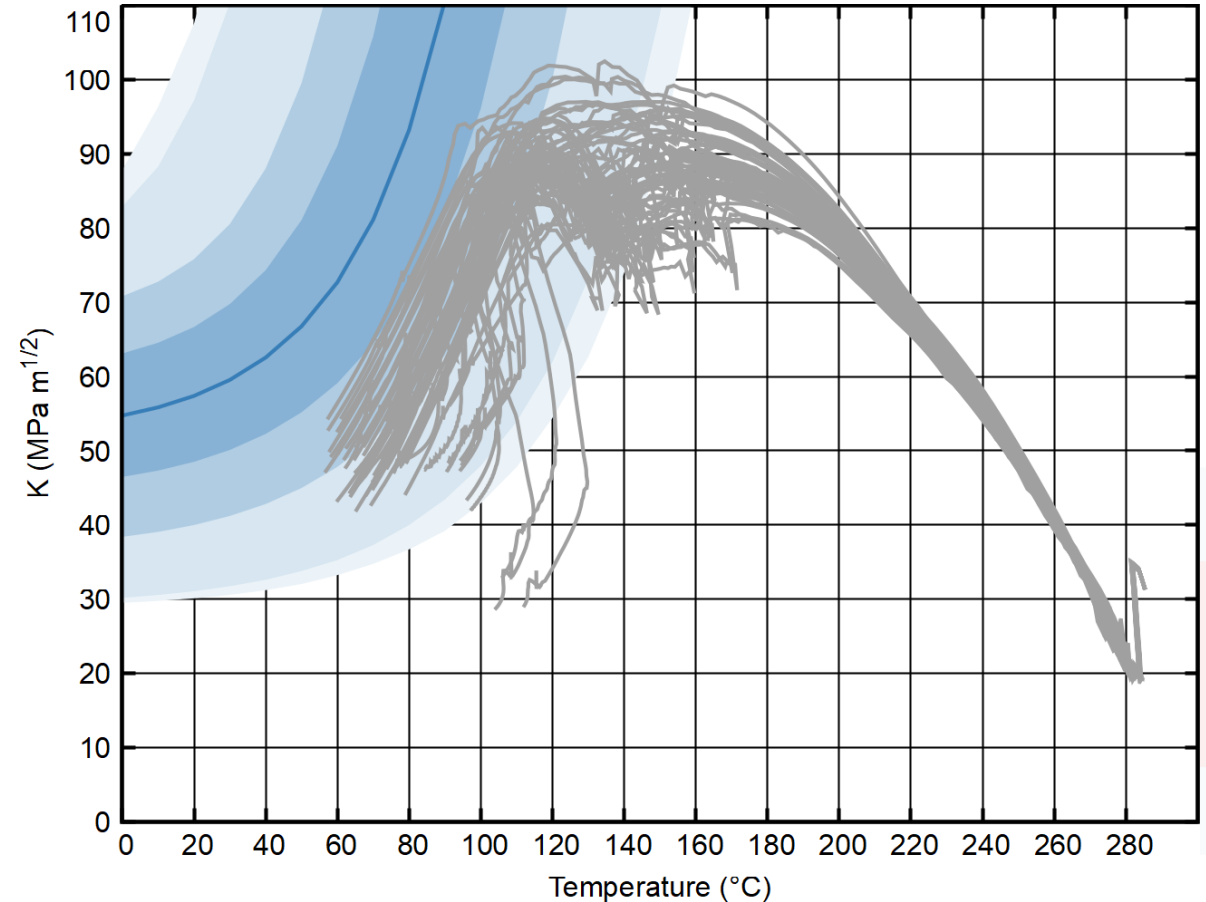
## Introduction

- Consideration of different sets of TH parameters
- Wilks argument: one-sided tolerance limit, lower bound
- Set of transients, depending on
  - Number of distributed parameters
  - Tolerance limit, lower bound
  - Rank
  - Usually: 59-130 transients



# Thermal-hydraulic uncertainties and probabilistics

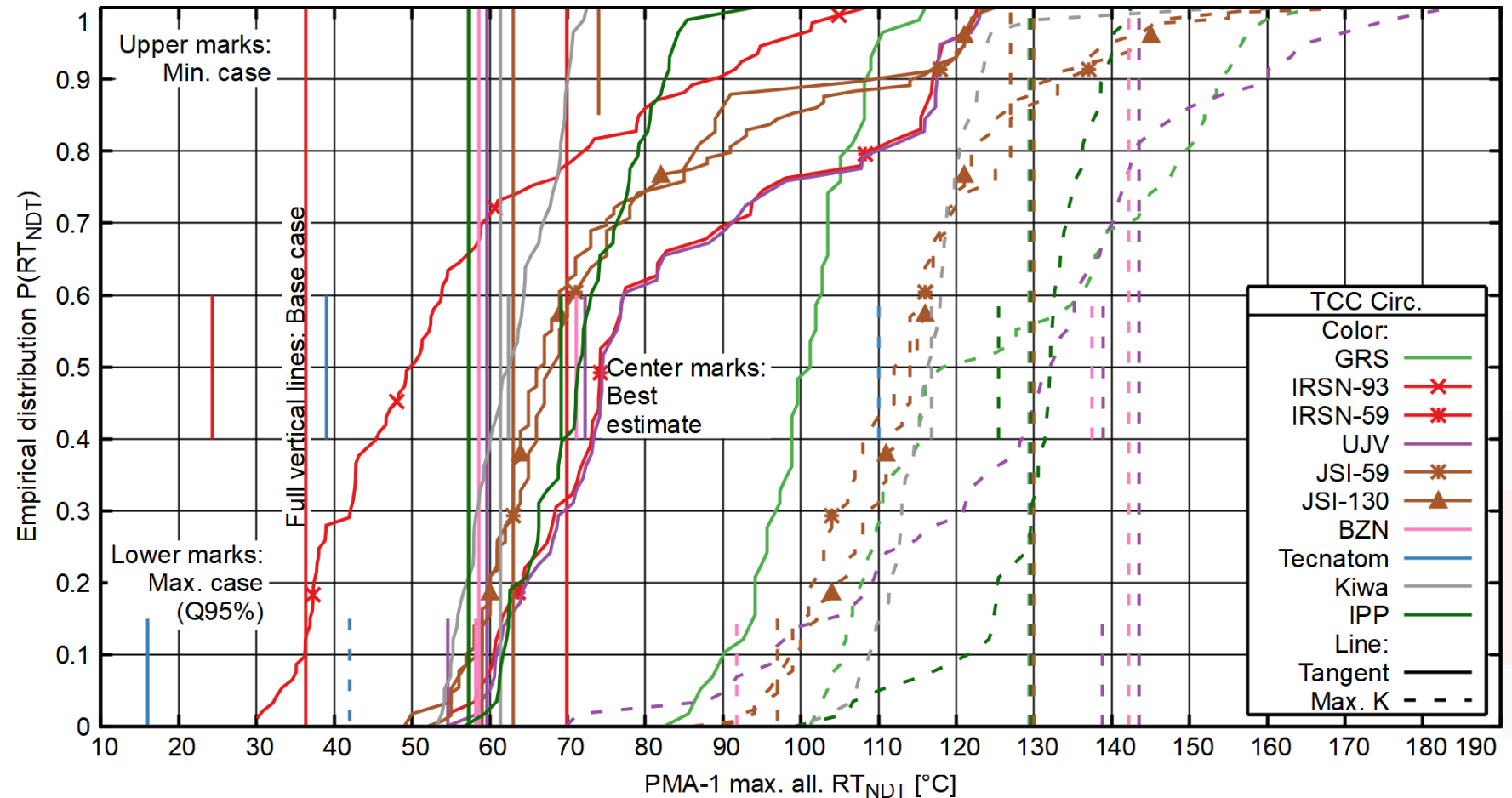
- Probabilistic Analysis of full Wilks set
  - First of a kind in APAL
  - Demanding (59-130 transients)!
- Apply margin to full set
  - Max. all. ref. temperature
  - Lifetime margin
- Derive cumulative distribution function (CDF) for margin





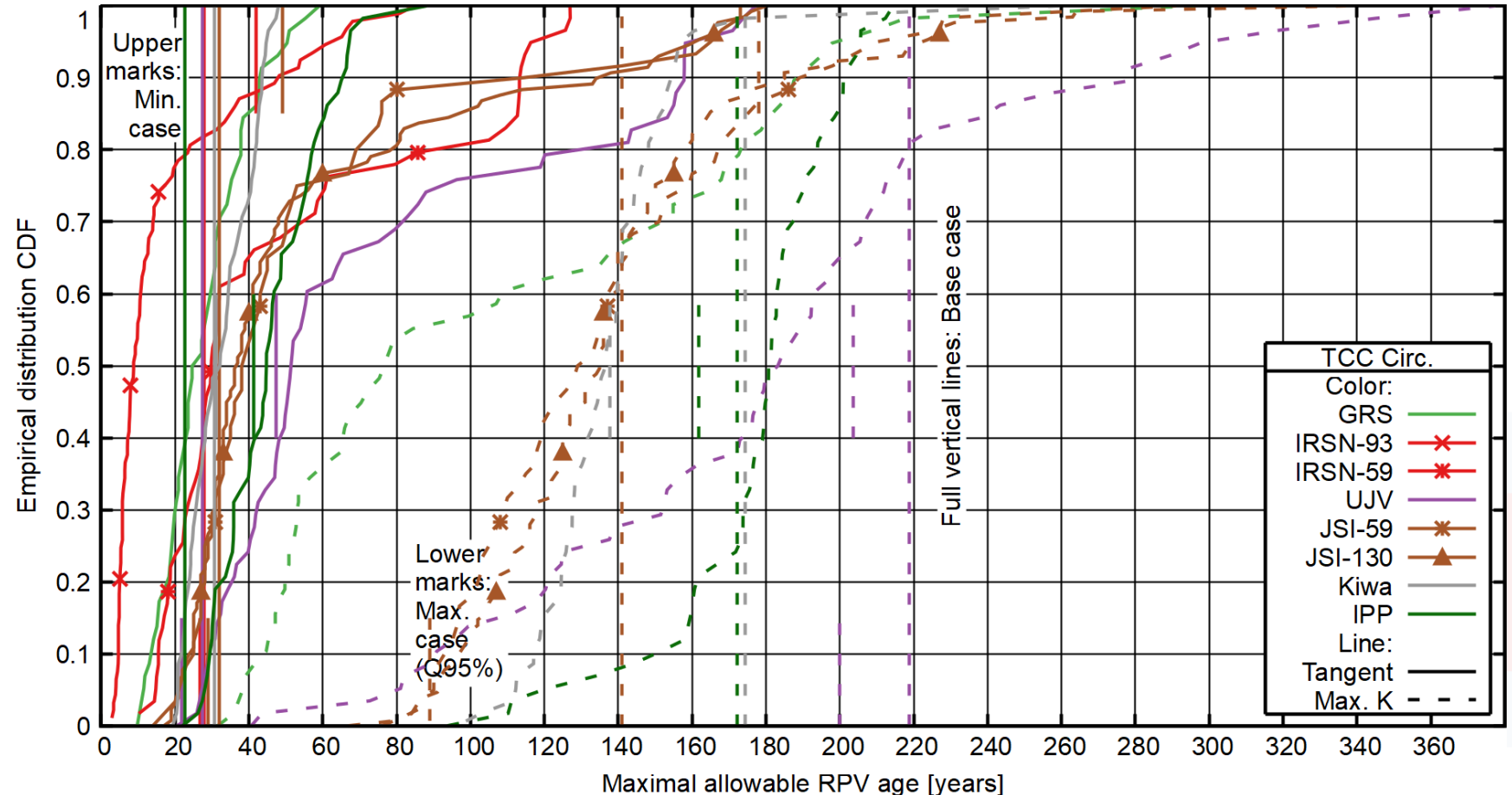
# Max. all. ref. Temperature: Full Wilks Set

- Different TH codes / data sets
- Consideration of 59-130 transients
- Empirical distribution function for margin  $RT_{NDT}$ 
  - 30-80 °C scatter
- Criterion:
  - Tangent
  - Max. K WPS



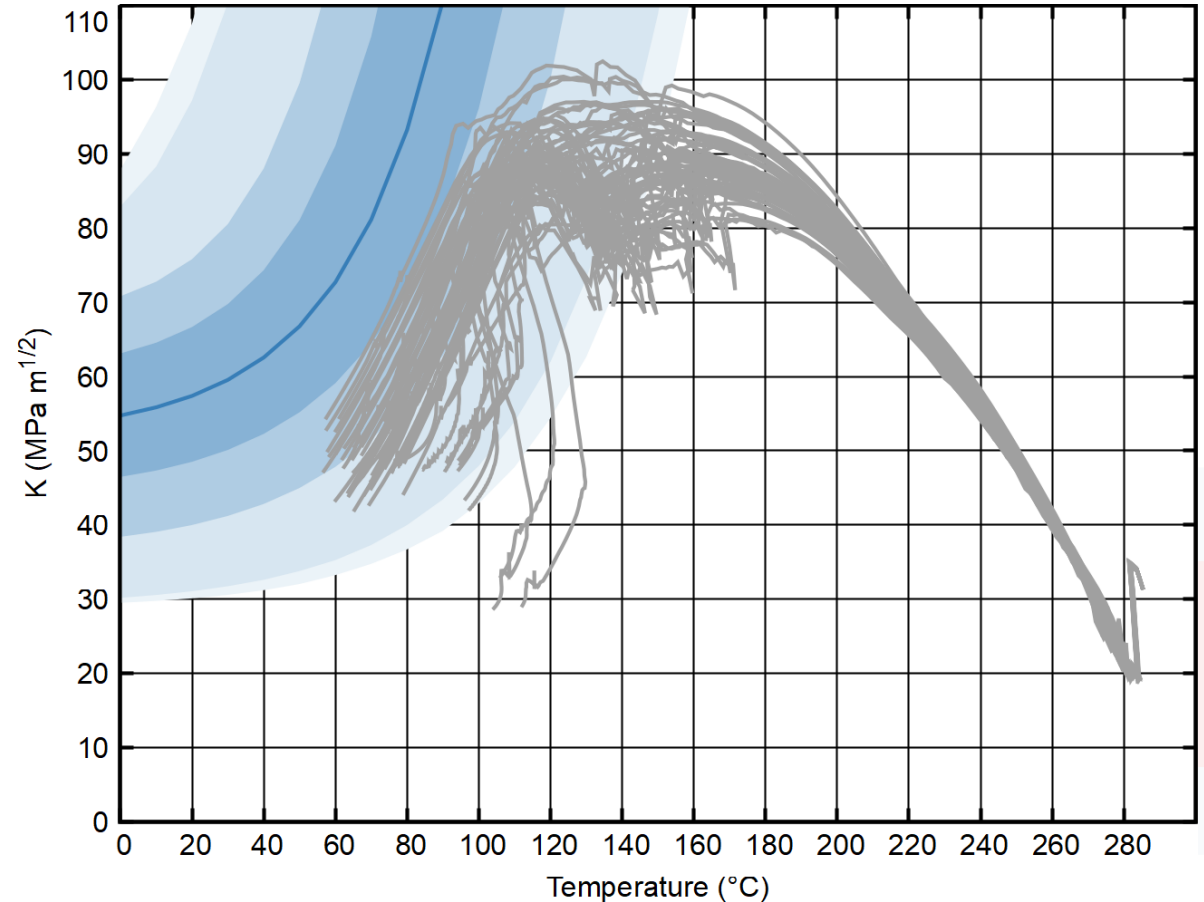
# Max. all. lifetime: Full Wilks set

- Different TH codes / data sets
- Consideration of 59-130 transients
- Empirical distribution function for margin
- Tangent
  - ~50-140 years scatter
- Max. K WPS
  - ~240-320 years scatter

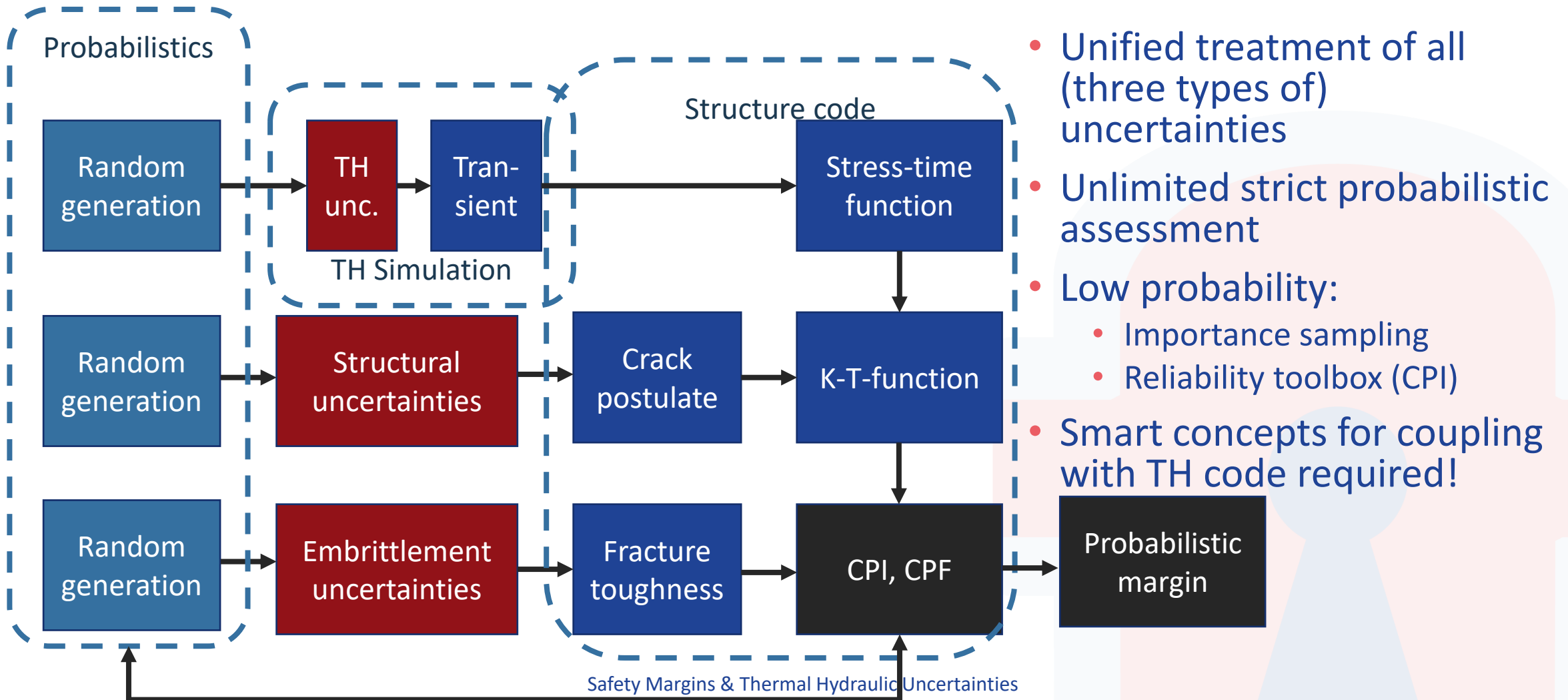


# The challenge

- Why not „integrating“ THU?
- Sketch: Simplistic Monte Carlo
  - Random sampling of „structural“ parameters
  - Random selection of transient from set
  - Monte Carlo summation
- Problem:
  - The sample size  $N$  of the TH transients is limited ( $N$  between 59 and 130)
  - The target CPI is usually much smaller than  $1/N$



# Vision: Integrated probabilistic approach



- Unified treatment of all (three types of) uncertainties
- Unlimited strict probabilistic assessment
- Low probability:
  - Importance sampling
  - Reliability toolbox (CPI)
- Smart concepts for coupling with TH code required!

# Final Summary

- Margin quantification
  - i. Assessment based on maximal allowable adjusted reference temperature
  - ii. Assessment based on lifetime
  - iii. Assessment based on reliability theory
- Thermal-Hydraulic Uncertainties
  - THU propagate to broad CDF for the margins
  - This shows the need for systematic consideration of THU in PTS assessment
  - Motivation for integrated probabilistic assessment
    - „Vision“ of integration of THU
    - Requires advanced sampling / reliability techniques for low target probability